

1 **In-situ  $V_p/V_s$  ratio reveals fault-zone material variation**  
2 **at the westernmost Gofar transform fault, East Pacific**  
3 **Rise**

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8 **Key Points:**

- 9 • Rupture barrier zone has a moderate  $V_p/V_s$  ratio of 1.75–1.80.  
10 • Down-dip edge of the 2008 *M*6 mainshock has a low  $V_p/V_s$  ratio of 1.61–1.69.  
11 •  $V_p/V_s$  ratio in the rupture barrier zone increased in the nine months before the  
12 mainshock.

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**Abstract**

Ocean transform faults often generate characteristic earthquakes that repeatedly rupture the same fault patches. The westernmost Gofar transform fault quasi-periodically hosts  $\sim M6$  earthquakes every  $\sim 5$  years, and microseismicity suggests that the fault is segmented into five distinct zones, including a rupture barrier zone that may have modulated the rupture of adjacent  $M6$  earthquakes. However, the relationship between the systematic slip behavior of the Gofar fault and the fault material properties is still poorly known. Specifically, the role of pore fluids in regulating the slip of the Gofar fault is unclear. Here, we develop a new method using differential arrival times between nearby earthquakes to estimate the in-situ  $V_p/V_s$  ratio of the fault-zone materials. We apply this technique to the dataset collected by an ocean-bottom-seismometer network deployed around the Gofar fault in 2008, which recorded abundant microearthquakes, and find a moderate  $V_p/V_s$  ratio of 1.75–1.80 in the rupture barrier zone and a low  $V_p/V_s$  ratio of 1.61–1.69 in the down-dip edge of the 2008  $M6$  rupture zone. This lateral variation in  $V_p/V_s$  ratio may be caused by both pore fluids and chemical alteration. We also find a 5–10% increase in  $V_p/V_s$  ratio in the barrier zone during the nine months before the mainshock. This increase may have been caused by fluid migrations or slip transients in the barrier zone.

**Plain Language Summary**

Oceanic transform faults are natural laboratory for studying earthquake processes because characteristic earthquakes on them are usually highly repeatable. One such example is the westernmost Gofar transform fault. The fault has two rupture zones regularly generating magnitude 6 earthquakes every 5 to 6 years, which are separated by a barrier zone repeatedly stopping ruptures on the two adjacent segments. One explanation for the barrier zone’s distinct behavior is that it consists of different materials from the rupture zones. To explore this hypothesis, we analyze records of thousands of small earthquakes that occurred in 2008 and find that the barrier zone has a higher ratio between P and S velocities than that of the rupture zone. This difference indicates that the materials in the barrier zone and the rupture zone are different in their fluid content and chemical composition, which may have regulated their distinct slip behaviors. We also find an increase in the ratio between P and S velocities in the barrier zone in the nine months before the magnitude 6 earthquake in 2008, which may reflect fluid flows or fault slips in the barrier zone.

**1 Introduction**

Oceanic transform faults demonstrate some of the most systematic and predictable slip behaviors. Moderate- to large-magnitude characteristic earthquakes often rupture the same fault patches quasi-periodically, which are frequently preceded by systematic foreshock activity (McGuire et al., 2005). This clear earthquake-cycle pattern implies that the underlying physical processes are likely repeatable. Therefore, oceanic transform faults are ideal natural laboratories for studying the mechanisms of earthquake nucleation and arrest (McGuire, 2008; Boettcher & McGuire, 2009). Specifically, their regular cycles provide opportunities to capture anticipated characteristic events and record variations in material properties that may reflect the stress and strength evolution leading to the characteristic earthquakes.

The Gofar transform-fault system at the East Pacific Rise (Fig. 1a) exemplifies such regular earthquake behaviors. The fault system has two short intra-transform spreading centers (ITSC) and three segments with the westernmost segment denoted as G3. The G3 segment, situated between the East Pacific Rise (EPR) in the west and an ITSC in the east (Fig. 1a), regularly hosts  $\sim M6$  events every  $\sim 5$  years at two separate asperities (McGuire, 2008). The two asperities are locked interseismically and are connected

63 by a  $\sim 10$  km long rupture barrier zone (hereafter “barrier zone”) along strike. The bar-  
 64 rier zone seems to have repeatedly stopped the ruptures of  $M6$  earthquakes at the locked  
 65 zones, including the Sep 18, 2008  $M6$  mainshock that occurred west of the barrier zone  
 66 (Fig. 1a–c; McGuire et al., 2012). The barrier zone is likely highly fractured with a fluid-  
 67 filled porosity up to 8% and has a  $\sim 10$ –20% P-wave velocity reduction extending through  
 68 the whole crust to the uppermost mantle, in contrast to the velocity structure of the rup-  
 69 ture zone (Roland et al., 2012; Froment et al., 2014). The average S-wave velocity of the  
 70 barrier zone decreased by about 3% and then fully recovered within one week prior to  
 71 the 2008  $M6$  mainshock, showing a dynamic evolution of the material properties (McGuire  
 72 et al., 2012; Froment et al., 2014). The observed velocity changes are likely related to  
 73 adjustments of poroelastic properties (e.g., fluid fraction and pore geometry) resulting  
 74 from stress changes (McGuire et al., 2012). However, details of the along-strike material-  
 75 property changes remain elusive primarily due to the limited spatial resolution of con-  
 76 ventional imaging techniques.

77 Rock  $V_p/V_s$  ratio is sensitive to both the pore fluids and the mineral composition  
 78 (Christensen, 1996; Takei, 2002). Specifically, in-situ  $V_p/V_s$  ratios obtained from differ-  
 79 ential P and S arrival times of nearby earthquakes are capable of resolving fault-zone ma-  
 80 terial properties with high spatial and temporal resolutions in the near-source regions  
 81 than conventional tomographic images (Lin & Shearer, 2007, 2009; Lin et al., 2015; Bloch  
 82 et al., 2018; Lin & Shearer, 2021). For example, Lin et al. (2022) showed that the high-  
 83 resolution in-situ  $V_p/V_s$  ratios are much more complex than the tomographic  $V_p/V_s$  mod-  
 84 els in California and that the in-situ  $V_p/V_s$  ratios illuminate the important role of flu-  
 85 ids in driving repeating earthquakes.

86 Here, we use an one-year ocean-bottom-seismometer (OBS) dataset recorded by  
 87 a 2008 experiment at G3, which captured the anticipated  $M6$  characteristic earthquake  
 88 as well as  $\sim 30,000$  microearthquakes, to investigate the variation of in-situ  $V_p/V_s$  ra-  
 89 tio in the fault zone. We design a new method to examine the spatio-temporal evolu-  
 90 tion of the in-situ  $V_p/V_s$  ratio and validate the method with a suite of synthetic tests.  
 91 We then compare the estimates with predictions from rock-physics models to infer phys-  
 92 ical processes within the G3 fault zone.

## 93 2 Data

94 We use the data collected by the 2008 Quebrada-Discovery-Gofar marine seismic  
 95 experiment (McGuire et al., 2012; Roland et al., 2012; Froment et al., 2014). The ex-  
 96 periment deployed 40 OBS stations, including 16 broadband seismographs around G3  
 97 (triangles in Fig. 1a). Among the 16 stations, three did not record useful data (gray tri-  
 98 angles in Fig. 1a), and thus our analysis focuses on the waveforms from the rest 13 sta-  
 99 tions, which were configured to sample at either 50 Hz or 100 Hz. We use the catalog  
 100 from Gong and Fan (2022) to estimate the in-situ  $V_p/V_s$  ratio of the G3 fault zone. The  
 101 catalog includes both automated and manually determined locations, and we focus on  
 102 the 30,854 earthquakes reported in the automated catalog in this study (see Gong and  
 103 Fan (2022) for details). The earthquakes are mostly within  $\pm 1$  km in the strike-normal  
 104 direction (Fig. 1a). We first obtain both P and S waveforms of the earthquakes, resam-  
 105 ple the waveforms to 100 Hz, and then bandpass filter the records at 4–20 Hz. The wave-  
 106 forms are windowed from -0.4 to 0.6 s around the predicted P arrivals and -0.8 to 0.7 s  
 107 around the predicted S arrivals. The predicted P and S arrivals are obtained using an  
 108 one-dimensional (1D) velocity model extracted from Roland et al. (2012). We cross-correlate  
 109 the P and S waveforms of each earthquake with those of its closest 100 neighboring events  
 110 recorded at the same station. The differential P and S traveltimes and cross-correlation  
 111 coefficients are computed for each event-pair at every available station, but they are only  
 112 recorded when cross-correlation coefficient of at least one phase is greater than 0.6. We  
 113 only keep cross-correlation measurements of an event pair if more than five stations can  
 114 meet the requirement. We note that the recording criteria are loose and additional se-

115 lection processes are necessary as discussed below. In total, we obtain 8,857,302 differ-  
 116 ential arrival times for estimating in-situ  $V_p/V_s$  ratios.

### 117 3 Methods

#### 118 3.1 Fault Patches of Interest

119 The  $\sim 30,000$  microearthquakes are nonuniformly distributed within the G3 fault  
 120 zone. To study the variation of the in-situ  $V_p/V_s$  ratio of the G3 fault zone, we focus on  
 121 ten non-overlapping patches. The selection is primarily guided by the spatio-temporal  
 122 evolution of seismicity reported in Gong and Fan (2022). The patches differ in their sizes  
 123 to balance the spatial resolution and a sufficient number of differential arrival times for  
 124 each patch (Figs. 1b and c). Only one  $V_p/V_s$  ratio is estimated for each patch for a time  
 125 period. For example, we divide the barrier zone into four patches due to its active seis-  
 126 micity, while grouping the east lock zone into one single patch because of its low seis-  
 127 micity. Regardless of the fault patch dimensions, we only use the differential arrival times  
 128 of event pairs within 2 km to obtain local in-situ  $V_p/V_s$ -ratio estimates. OBS data of-  
 129 ten have inaccurate timing because the instrument clocks are unable to synchronize with  
 130 satellites. Although a linear clock correction has been applied to the data when the data  
 131 was archived, the residual nonlinear clock drift may still bias the results (Gouédard et  
 132 al., 2014). Therefore, we only use event pairs occurring within 30 days to minimize the  
 133 effects of the clock drifts. We further evaluate the impacts of the maximum event tem-  
 134 poral separation in Section 5.1.1.

135 The eastern G3 hosted an  $M6$  event in 2007 (approximately Zone 1 in Gong and  
 136 Fan (2022); McGuire et al. (2012)). Because this fault segment had only 2,487 earthquakes  
 137 during the observational period, we group them into one patch (Patch E; Figs. 1b and  
 138 c). The barrier zone (approximately Zone 2 in Gong and Fan (2022)) includes four patches  
 139 with two shallow patches F1 and F2 and two deep patches D1 and D2, where the seis-  
 140 micity rate was high before the mainshock but largely halted after the mainshock (Figs. 1b  
 141 and c). We define two patches M1 and M2 at the down-dip edge of the mainshock rup-  
 142 ture zone (approximately Zone 3 in Gong and Fan (2022); the rupture zone is largely qui-  
 143 escent before and after the mainshock), with M1 being seismically active during the whole  
 144 observation period and M2 consisting mostly aftershocks of the 2008  $M6$  earthquake (Figs. 1b  
 145 and c). We note that M2 and F1 are spatially close but have distinct temporal patterns  
 146 of seismicity (Gong & Fan, 2022), which implies a possible difference in material prop-  
 147 erties. The events immediately west of the mainshock zone are grouped into the patch  
 148 T (approximately Zone 4 in Gong and Fan (2022)), where a moderate level of seismic-  
 149 ity persisted through the observational period (Figs. 1b and c). The  $M6$  mainshock may  
 150 have also ruptured the area above T if the rupture propagated bilaterally (Figs. 1b and  
 151 c). Near the East Pacific Rise, the western end of G3 hosted a two-week long swarm in  
 152 December 2008, including two  $M5$  earthquakes (“December swarm” in McGuire et al.  
 153 (2012); approximately Zone 5 in Gong and Fan (2022)). This segment is divided into two  
 154 patches S1 and S2 (Figs. 1b and c).

#### 155 3.2 Preprocessing of Differential Arrival Times

156 In an ideal case where events occur in a homogeneous medium, and the measure-  
 157 ments contain no error or noise, the P and S differential arrival times of event pairs in  
 158 a compact cluster form a line with zero intercept and a slope equal to the  $V_p/V_s$  ratio  
 159 of the medium (e.g., Figure 3 in Lin and Shearer (2007)). In reality, the event origin times  
 160 are often not accurate enough, and these event-timing errors will introduce static time  
 161 shifts to the measured P and S differential arrival times. The time shifts will cause the  
 162 differential times to form lines with the same slope as the ideal case but varying inter-  
 163 cepts for different event pairs (e.g., Figure 5 in Lin and Shearer (2007)). Moreover, be-  
 164 cause our differential arrival times are computed without analyst reviews, the measure-

165 ments are susceptible to phase misalignment and other sources of random noise, which  
 166 could potentially bias the in-situ  $V_p/V_s$ -ratio estimates (see Section 5.1.1 for a detailed  
 167 discussion). For example, the measured differential arrival times for D1 are not only highly  
 168 scattered but also form a trend with a slope of  $\sim 1.3$ , significantly smaller than the  $V_p/V_s$   
 169 ratios of typical rocks (Fig. 2a). Therefore, we design a preprocessing procedure to re-  
 170 duce the effects of observation errors in differential arrival times before estimating in-  
 171 situ  $V_p/V_s$  ratios (Fig. 3).

172 We first remove arrival-time measurements with a cross-correlation coefficient less  
 173 than 0.6 for either P or S wave (e.g., Lin et al., 2007). We define this step as the CC step  
 174 and the following step as the linearity step because the following steps will further se-  
 175 lect the measurements based on how well they can be fitted with lines (Fig. 3). We then  
 176 fit differential arrival times of each event pair with a line while allowing for a non-zero  
 177 intercept and remove the intercept for the event pair (Fig. 3). For the line fitting, we re-  
 178 quire a minimum number ( $N_{\min}$ ) of seven data points and keep event pairs with a num-  
 179 ber of data points greater than the threshold for the following analysis. The threshold  
 180 is determined as  $N_{\min} = 7$  through trial-and-error, and its effect on the in-situ  $V_p/V_s$ -  
 181 ratio estimates will be discussed in Section 4.1. We iteratively fit a line for an event pair  
 182 using the total-least-square (TLS) regression (also known as “orthogonal-distance regres-  
 183 sion”; Van Huffel and Vandewalle (1991)), which minimizes the  $\ell_2$  norm of the misfits  
 184 for both the P and S differential times. All measurements of an event pair are initially  
 185 used to estimate a slope and an intercept, and a root-mean-square (RMS) misfit is recorded.  
 186 If the RMS misfit is below a threshold ( $\text{RMS}_{\max}$ ), we retain the measurements, remove  
 187 the estimated intercept from them, and record the slope estimate as the  $V_p/V_s$  ratio es-  
 188 timate for this event pair. Otherwise, we discard the data point with the largest misfit  
 189 and repeat the line fitting procedure. This iterative process is terminated when the RMS  
 190 misfit is below  $\text{RMS}_{\max}$  or the number of measurements of the event pair drops below  
 191  $N_{\min}$ . In the latter case, this event pair will not be used for further analysis. We choose  
 192 a threshold of  $\text{RMS}_{\max} = 0.005$  s, a strict criterion given the data sampling interval of  
 193 0.01 s. This parameter choice aims to retain only the highest-quality differential arrival  
 194 times for robust estimation. We will also evaluate the effects of different choices of  $\text{RMS}_{\max}$   
 195 in Section 4.1.

196 We use the joint distribution between the  $V_p/V_s$  ratios and differential-P-time ranges  
 197 ( $\tau$ ) of event pairs to further remove measurement outliers for each fault patch (Fig. 4).  
 198 The differential-P-time range  $\tau$  is defined as the difference between the maximum and  
 199 minimum differential P arrival times ( $\tau = \Delta T_{p,\max} - \Delta T_{p,\min}$ ) for an event pair. For  
 200 example, Fig. 4 shows the joint distributions for M1 and D1 after the intercept removal  
 201 step. The distributions show measurements forming apparent strips with  $V_p/V_s \approx 0$  and  
 202  $\tau > 0.15$  s (Fig. 4), which are clearly erroneous and thus excluded from further anal-  
 203 ysis. The remaining measurements are distributed in  $\tau = 0.001\text{--}0.150$  s and  $V_p/V_s =$   
 204  $0.5\text{--}3$  (Fig. 4). This group centers around 1.7 and shows a variation decreasing with in-  
 205 creasing  $\tau$  (Fig. 4). We opt to use event pairs with  $V_p/V_s = 0.5\text{--}3$  and  $\tau = 0.050\text{--}0.150$  s  
 206 (solid green boxes in Fig. 4) for estimating  $V_p/V_s$  ratios. The  $V_p/V_s$ -ratio range in our  
 207 criteria removes measurements that would lead to erroneous estimates, and the  $\tau$  limit  
 208 helps select event pairs with reliable estimates. The lower bound for  $\tau$  ( $\tau_{\min}$ ) is a key  
 209 parameter because it controls the trade-off between data quantity and quality, and we  
 210 will discuss its effect in detail in Section 4.1.

211 The preprocessing procedure removes most of the cross-correlation measurements  
 212 and retains only a small portion (typically  $< 1\%$ ) of the data points. However, the se-  
 213 lected measurements have high quality and likely yield more accurate estimates. For ex-  
 214 ample, the unprocessed measurements of D1 show strong scattering and a trend with a  
 215 slope of  $\sim 1.3$ , whereas the preprocessed measurements yield a best-fitting line with a  
 216 slope of  $\sim 1.8$  (Figs. 2a and b). Elaborate preprocessing could potentially cause selec-  
 217 tion biases, i.e., our strict data-selection procedure could bias the  $V_p/V_s$ -ratio estimates.

218 However, we emphasize that the line-fitting step of the preprocessing procedure does not  
 219 limit the slope ( $V_p/V_s$  ratio) values and that the joint-distribution-analysis step selects  
 220 event pairs in a generous range of  $V_p/V_s = 0.5\text{--}3$  (Fig. 4). We will further test the ef-  
 221 fects of the preprocessing procedure on synthetic data to show that it does not introduce  
 222 biases to the final  $V_p/V_s$ -ratio estimates (Section 5.1.1). Among all fault patches, the patches  
 223 in the swarm zone (S1 and S2) have a remarkably lower fraction of events left for the fi-  
 224 nal  $V_p/V_s$ -ratio estimation compared to other patches (Fig. 1d). Besides, the remain-  
 225 ing events in F2 after preprocessing are predominantly located in the deeper part of the  
 226 patch (Fig. 1d). These features are probably because both the swarm and barrier zones  
 227 have high degrees of structural complexity due to pervasive fracturing, which could lead  
 228 to incoherent waveforms between events, causing their differential arrival times to have  
 229 larger errors and thus be eliminated in the preprocessing procedure. We will further dis-  
 230 cuss the relation between data retention rate and structural complexity in Section 5.3.1.

### 231 3.3 Robust $V_p/V_s$ -ratio Estimation

232 With the selected differential arrival times, we estimate the in-situ  $V_p/V_s$  ratio for  
 233 each fault patch following an iterative approach similar to the line-fitting step in the pre-  
 234 processing procedure. We first fit a line with zero intercept to the measurements and com-  
 235 pute the standard deviation of the misfits and remove the measurements with a misfit  
 236 greater than two times the standard deviation. We then repeat the line-fitting using the  
 237 remaining measurements to obtain the final  $V_p/V_s$  ratio estimate. This data removal step  
 238 typically disqualify less than 10% of the measurements, and the  $V_p/V_s$  ratios estimated  
 239 at the two steps are only marginally different (Figs. 2b and c). We further estimate the  
 240 uncertainties of the  $V_p/V_s$ -ratio estimates by computing the standard deviation of the  
 241  $V_p/V_s$  ratios from 500 bootstrap-resampled datasets. Each bootstrap realization is ob-  
 242 tained by randomly drawing the same number of measurements from the original dataset  
 243 with replacement, allowing the same measurement to be sampled multiple times. We note  
 244 that the uncertainty estimate from bootstrap resampling provides a measure of data vari-  
 245 ability yet does not address uncertainties resulting from choices of preprocessing param-  
 246 eters or the spatial resolution of our data and method (Section 5.1). As an example, the  
 247 final  $V_p/V_s$  ratio for D1 is estimated to be 1.799 with an uncertainty of  $\pm 0.006$  and an  
 248 RMS misfit of 0.005 s.

## 249 4 Results

### 250 4.1 Spatial Variation of In-situ $V_p/V_s$ Ratio

251 The in-situ  $V_p/V_s$ -ratio estimates of the ten fault patches show a distinct spatial  
 252 variation with values ranging from 1.524 to 1.799. The eastern part of G3, including the  
 253 barrier zone (F1, F2, D1, and D2) and the eastern locked zone (E), have high  $V_p/V_s$  ra-  
 254 tios (1.752–1.799), whereas the western part, including the mainshock zone (M1 and M2),  
 255 the transition zone (T), and the eastern patch of the swarm zone (S2), have low  $V_p/V_s$   
 256 ratios (1.524–1.693; Fig. 1d). The other fault patch S1 in the swarm zone has a  $V_p/V_s$   
 257 ratio of 1.777, similar to the patches in the east (Fig. 1d). S1 and S2 have much fewer  
 258 event pairs for estimating  $V_p/V_s$  ratio compared to the other patches probably due to  
 259 the combined effects of a poor station coverage and dissimilarity of event waveforms (Figs. 1a  
 260 and d). Due to the low number of measurements, results for S1 and S2 are likely less re-  
 261 liable than those of other fault patches and thus will not be further discussed. We ob-  
 262 serve a sharp contrast in  $V_p/V_s$  ratio between the two adjacent patches M2 and F1, which  
 263 correlates with the temporal variation of their seismicity (Figs. 1b–d; Gong & Fan, 2022).  
 264 These observations suggest an abrupt boundary in material properties between the main-  
 265 shock zone and the barrier zone. The in-situ  $V_p/V_s$  ratios, their uncertainties, and as-  
 266 sociated RMS misfits of all fault patches except for S1 and S2 are summarized in Table S1.

267 To evaluate the robustness of the observed spatial variation, we examine the effects  
 268 of  $N_{\min}$ ,  $\text{RMS}_{\max}$ , and  $\tau_{\min}$  on the  $V_p/V_s$  ratio estimates. We test the effects of these pa-  
 269 rameters by only varying one parameter at a time while keeping the other two at our pre-  
 270 ferred values of  $N_{\min} = 7$ ,  $\text{RMS}_{\max} = 0.005$  s, and  $\tau_{\min} = 0.05$  s, leading to six addi-  
 271 tional sets of parameter combinations for the eight fault patches (except for S1 and S2;  
 272 5). For  $N_{\min}$ , we test  $N_{\min} = 5, 7$ , and 9 (Figs. 1d and 5a), and the results suggest a  
 273 negative correlation between the  $V_p/V_s$ -ratio estimates and  $N_{\min}$ . However, the relative  
 274 differences of the  $V_p/V_s$ -ratio estimates remain largely unchanged, indicating that the  
 275 observed spatial pattern is robust. For example, the  $V_p/V_s$  ratios of M2 and F1 both de-  
 276 crease as  $N_{\min}$  increases from 5 to 9, but the estimate of M2 remains smaller than that  
 277 of F1 (Figs. 1d and 5a). The general decrease of the estimates with increasing  $N_{\min}$  may  
 278 be because a greater  $N_{\min}$  reduces the number of measurements with large differential-  
 279 arrival-time values, which have stronger impacts on the  $V_p/V_s$  estimates than the mea-  
 280 surements closer to the origin. Including large differential-arrival-time measurements could  
 281 yield more robust estimates because random errors in these measurements are smaller  
 282 compared with the measurements themselves. The  $V_p/V_s$ -ratio estimates for M1, D1, and  
 283 D2 are largely insensitive to the choice of  $N_{\min}$  likely due to their more numerous mea-  
 284 surements (Figs. 1d and 5a).

285 We vary  $\text{RMS}_{\max}$  from 0.005 s to 0.015 s and find that the  $V_p/V_s$ -ratio estimates  
 286 are generally insensitive to the choice of the parameter (Figs. 1d and 5b). For  $\tau_{\min}$ , we  
 287 vary its value from 0.025 to 0.075 s and find that the  $V_p/V_s$ -ratio estimates positively cor-  
 288 relate with  $\tau_{\min}$ , although the spatial variation of the estimates remain the same (Figs. 1d  
 289 and 5c). The positive correlation may be because a greater  $\tau_{\min}$  tends to select more mea-  
 290 surements with large differential arrival times, which influences the  $V_p/V_s$ -ratio estimates  
 291 in an opposite way to that of  $N_{\min}$ . This suite of sensitivity tests demonstrates that al-  
 292 though the absolute  $V_p/V_s$  ratios are affected by the parameters, the resolved spatial vari-  
 293 ation in  $V_p/V_s$  ratio is robust regardless of the preprocessing-parameter choices.

## 294 4.2 Temporal Evolution of In-situ $V_p/V_s$ Ratio

295 The fault patches in the mainshock zone (M1 and M2) and barrier zone (F1, F2,  
 296 D1, and D2) have sufficient measurements to enable us to evaluate the temporal evolu-  
 297 tion of  $V_p/V_s$  ratios in these segments (Fig. 6). For each fault patch, we group every 50  
 298 consecutive event pairs (after preprocessing) into a time window with a temporal incre-  
 299 ment of 10 event pairs. This scheme creates nonuniform window lengths but an equal  
 300 number of measurements for each window, which guarantees that the estimates are ro-  
 301 bust and that the observed temporal variation is not due to a change in sample size. We  
 302 then estimate the  $V_p/V_s$  ratio for each time window and evaluate its temporal variation.  
 303 Because the temporal variation of seismicity is very different between different patches,  
 304 the distribution of time windows also varies greatly between them (Fig. 6). Regardless  
 305 of the time window length, only differential-time measures of event pairs within 30 days  
 306 are used for estimating  $V_p/V_s$  ratios.

307 The estimated in-situ  $V_p/V_s$  ratios fluctuate at all six fault patches albeit with dif-  
 308 ferent magnitudes. The  $V_p/V_s$  ratio of M1 oscillates within  $\pm 3\%$  of the average value and  
 309 shows no clear trend during the observation period (Figs. 6a and 7b). The  $V_p/V_s$  ratio  
 310 of M2 appears to have decreased  $\sim 3\%$  after the mainshock, though this change may  
 311 not be well resolved due to a lack of earthquakes in M2 before the  $M6$  mainshock (Figs. 6b  
 312 and 7b). In contrast, the four barrier-zone patches, F1, F2, D1, and D2, show a greater  
 313 fluctuation with an apparent increasing trend before the  $M6$  mainshock (Figs. 6c–e and  
 314 7a). Hereafter, we will use Julian day (abbreviated as d; number of days since Jan 1, 2008)  
 315 to describe the temporal evolution of the in-situ  $V_p/V_s$  ratios. For F1, the  $V_p/V_s$  ratio  
 316 increased by  $\sim 6\%$  between  $\sim 60$  and  $\sim 120$  d, dropped by  $\sim 5\%$  between  $\sim 120$  and  
 317  $\sim 160$  d, and increased again by  $\sim 5\%$  between  $\sim 160$  d and the mainshock (Figs. 6c  
 318 and 7a). For F2, the  $V_p/V_s$  ratio increased by  $\sim 9\%$  between  $\sim 30$  and  $\sim 100$  d, dropped

by  $\sim 5\%$  between  $\sim 100$  and  $\sim 120$  d, and then increased by  $\sim 3\%$  between  $\sim 120$  and  $\sim 160$  d (Figs. 6d and 7a). Although F2 had abundant microearthquakes before the mainshock, a lower percentage of their differential arrival times passed the preprocessing procedure compared to other barrier-zone patches, resulting in a lack of measurements in the 100 days immediately before the mainshock (Fig. 6d). For D1, we observe a nearly-monotonic increase in  $V_p/V_s$  before the mainshock with a cumulative change of  $\sim 10\%$  (Figs. 6e and 7a). In contrast, the  $V_p/V_s$  ratio of D2 dropped by  $\sim 5\%$  between  $\sim 30$  and  $\sim 80$  d and then gradually increased by  $\sim 4\%$  in the remaining time before the mainshock (Figs. 6f and 7a). The changes in  $V_p/V_s$  ratio in the barrier-zone (Figs. 1b and 6c–f) may be related to pore-fluid migration or slip transients as suggested by the intense foreshocks in the barrier zone (McGuire et al., 2012; Gong & Fan, 2022).

### 4.3 3D Synthetic Tests

#### 4.3.1 Validation of Spatial Variation

In-situ  $V_p/V_s$  ratio estimates are generally free of biases if the earthquakes have an isotropic distribution and the  $V_p/V_s$  ratio varies smoothly with depth (Lin & Shearer, 2007). Nonetheless, complex three-dimensional (3D) velocity structures may bias the estimates, although such effects depend on the velocity structure, event distribution, and network configuration (Palo et al., 2016). At G3, the barrier zone has a significantly lower  $V_p$  compared to the surrounding oceanic lithosphere (Roland et al., 2012), and our results as well as previous studies also suggest a strong along-strike velocity variation (Froment et al., 2014; Guo et al., 2018). Furthermore, the earthquakes are primarily distributed along strike with a narrow strike-normal spread (Fig. 1a). Given these complications, we perform synthetic tests using 3D velocity models to evaluate their effects on the in-situ  $V_p/V_s$ -ratio estimates.

We test three 3D velocity models consisting of a vertical fault zone embedded in the oceanic lithosphere (Figs. 8, 9, and S1). The oceanic lithosphere has the same 1D  $V_p$  profile as the one used for locating the earthquakes (Figs. 8a, 9a, and S1a; Gong and Fan (2022)). We set the  $V_p/V_s$  ratio of the oceanic lithosphere to decrease exponentially from 2.00 at the seafloor to 1.73 at infinite depth (Figs. 8b, 9b, and S1b). This  $V_p/V_s$ -ratio profile is consistent with those of the oceanic lithosphere derived from active-source experiments (e.g., Spudich & Orcutt, 1980). The fault zone has a uniform, low  $V_p$  of  $5 \text{ km s}^{-1}$  in all the models, which is obtained from Roland et al. (2012) (Figs. 8a, 9a, and S1a). The fault zone is extended to 10 km deep (Figs. 8a and b, 9a and b, and S1a and b) to match the deep seismicity in D1 and D2 (Figs. 1b–d). To assess the effects of the event and station distributions, we use the same station locations and the same earthquakes that are used for estimating the in-situ  $V_p/V_s$  ratios (Figs. 8a–c, 9a–c, and S1a–c). We compute synthetic P and S travel times using PyKonal (White et al., 2020), which can efficiently compute travel times and ray paths in 3D models. We then estimate the  $V_p/V_s$  ratios from the synthetic travel times and compare them with the input values (Figs. 8d, 9d, and S1d).

Model 1 has a homogeneous fault zone with a  $V_p/V_s$  ratio of 1.70 and a width of 5 km (Figs. 8a–c), which is similar to the fault-zone width reported in Roland et al. (2012). The results show that the  $V_p/V_s$ -ratio estimates are close to the input value despite being slightly elevated on average (Fig. 8d). The deviations of the estimated values are smaller than 2% from the input values and show no spatial pattern (Fig. 8d). The small deviations are likely due to the smearing effects from the wall rock, which has a higher  $V_p/V_s$  ratio at the depths of the events ( $\sim 1.75$ ; Figs. 8b and c). These results demonstrate that the observed  $V_p/V_s$ -ratio contrast between the barrier zone and the mainshock zone is unlikely an artifact due to the source-receiver configuration.

In Model 2, we use a fault zone width of 5 km and assign a low  $V_p/V_s$  ratio of 1.70 to the western fault zone, which contains S1, S2, T, M1, and M2, and a high  $V_p/V_s$  ra-

370 tio of 1.80 to the eastern fault zone, which contains F1, F2, D1, D2, and E (Figs. 9b and  
 371 c). This  $V_p/V_s$ -ratio contrast imitates the observed  $V_p/V_s$ -ratio difference between the  
 372 mainshock zone and the barrier zone (Fig. 1d). The fault zone is kept to have a homo-  
 373 geneous  $V_p$  of  $5 \text{ km s}^{-1}$  (Fig. 9a). We find that the contrast in  $V_p/V_s$  ratio between the  
 374 two segments are well recovered (Fig. 9d). Similar to Model 1, smearing effects from the  
 375 wall rock likely cause the  $V_p/V_s$  ratios of the western and eastern segments to be slightly  
 376 overestimated and underestimated, respectively (Fig. 9d). These results demonstrate that  
 377 given the source-receiver configuration, an along-strike  $V_p/V_s$ -ratio variation similar to  
 378 the observation can be resolved with our method.

379 To assess the resolution of our method, we set Model 3 to have the same along-strike  
 380  $V_p/V_s$ -ratio variation as Model 2 but a fault-zone width of 2 km (Figs. S1a–c). This value  
 381 is the lower bound of the fault-zone width reported in Roland et al. (2012). For this case,  
 382 the estimated  $V_p/V_s$  ratios of all fault patches are close to 1.75, the  $V_p/V_s$  ratio of the  
 383 wall rock at the event depths, without a clear difference between the two segments (Fig. S1d).  
 384 This example highlights that the smearing effect of the surrounding materials can sig-  
 385 nificantly affect the  $V_p/V_s$ -ratio estimates of the fault-zone materials when the fault zone  
 386 is too narrow. We will further discuss the uncertainty caused by 3D velocity structures  
 387 in Section 5.1.2.

### 388 **4.3.2 Validation of Temporal Variation**

389 We further design Model 4 and Model 5 to validate the the apparent  $V_p/V_s$ -ratio  
 390 increase in the barrier zone (F1, F2, and D1). Specifically, we compute the synthetic travel  
 391 times for the first and the last time windows of the three patches using the true event  
 392 locations. We then estimate the  $V_p/V_s$  ratios using the synthetic data and compare them  
 393 with the input values. We set Model 4 to have the same velocity structure as Model 1  
 394 at both the first and last time windows, i.e., Model 4 is time invariant (Fig. 10a). The  
 395 estimated  $V_p/V_s$  ratios show no change over time, although the values of both time win-  
 396 dows are slightly overestimated as observed in the case of Model 1 (Figs. 8d and 10a).  
 397 These results demonstrate that the observed temporal change in  $V_p/V_s$  ratio in the bar-  
 398 rier zone (F1, F2, and D1) is unlikely an artifact caused by a change in event distribu-  
 399 tion over time. Finally, we use Model 5 to test the resolvability of a temporal change in  
 400  $V_p/V_s$  ratio similar in size and duration to the observations. Model 5 has the same ve-  
 401 locity structure as Model 1 in the first time window and changes to Model 2 in the sec-  
 402 ond window, i.e., the  $V_p/V_s$  ratio of the eastern fault zone increases from 1.70 to 1.80  
 403 (Fig. 10b). We find that the  $V_p/V_s$ -ratio changes of all three patches are well recovered  
 404 with marginal differences from the input values (Fig. 10b). These two tests show that  
 405 the observed  $V_p/V_s$ -ratio increase in the barrier zone is unlikely an artifact and that an  
 406  $V_p/V_s$ -ratio increase in the barrier zone is resolvable with our method and data.

## 407 **5 Discussions**

### 408 **5.1 Uncertainty Analyses**

409 We evaluate uncertainties in the in-situ  $V_p/V_s$ -ratio estimates resulting from two  
 410 main sources: noise and model assumptions.

#### 411 **5.1.1 Uncertainty from Noise**

412 The noise in the differential arrival-time data has three major components: instru-  
 413 ment clock drifts, event-timing errors, and cross-correlation alignment errors. Although  
 414 the linear time drifts in the OBS data were removed (Gouédard et al., 2014), significant  
 415 nonlinear time drifts may still be present and could bias the  $V_p/V_s$  ratio estimates. To  
 416 evaluate the potential impacts of instrument clock drifts, we estimate the  $V_p/V_s$  ratios  
 417 for the five fault patches in the mainshock zone and barrier zone (M1, M2, F1, F2, D1,

418 and D2) using different maximum temporal separations between event pairs of 15, 30,  
 419 45, and 60 days (Fig. 11). The results show that the  $V_p/V_s$  ratio estimates decrease slightly  
 420 ( $< 4\%$ ) with increasing maximum event temporal separation, although the relative dif-  
 421 ference between the patches largely remains the same (Fig. 11). Event pairs with large  
 422 event temporal separations likely suffer greater errors due to clock drifts. Such instru-  
 423 ment clock drifts introduce the same bias to both the P and S differential arrival times,  
 424 causing the  $V_p/V_s$  ratio estimates to converge towards 1, which may explain the nega-  
 425 tive correlation between the estimated  $V_p/V_s$  ratios and the maximum event temporal  
 426 separation. Given that the  $V_p/V_s$  ratios estimated using the preferred maximum event  
 427 temporal separation (30 days) do not differ significantly from those estimated using a  
 428 smaller maximum event temporal separation (15 days; Fig. 11), we conclude that the  
 429 results are unlikely biased by instrument clock drifts.

430 In theory, event-timing errors can be estimated and removed from the data. How-  
 431 ever, other types of noise, especially the cross-correlation alignment errors, can compli-  
 432 cate corrections for such errors in reality. As the first step of the quality-control process,  
 433 removing differential arrival times with low cross-correlation values ( $< 0.6$ ; Fig. 3) can-  
 434 not fully eliminate cross-correlation measurement errors, which is likely due to misalign-  
 435 ment between different phases (e.g., P and S; Fig. S2). Microearthquakes typically have  
 436 short body wave pulses, and bandpass-filtered P and S waves may have similar waveforms.  
 437 For example, aligning a P phase with the associated S phase will yield an erroneous dif-  
 438 ferential arrival time but a high cross-correlation value, causing outliers in the measure-  
 439 ments (Fig. 2a). We thus designed the linearity step in the preprocessing procedure to  
 440 further eliminate these outliers while also removing the event-timing errors (Figs. 3 and  
 441 4).

442 Since the preprocessing procedure removes the majority of the measurements (Fig.  
 443 2), one concern is if this procedure could bias the estimated  $V_p/V_s$  ratios. To evaluate  
 444 this possibility, we generate differential P and S arrival times assuming a  $V_p/V_s$  ratio of  
 445 2.00, an extreme value for rocks, and add synthetic event-timing errors, Gaussian ran-  
 446 dom noise, and outliers step by step to generate three sets of synthetic data (Fig. 12).  
 447 The event-timing errors and Gaussian noise are randomly generated from Gaussian distri-  
 448 butions with a zero mean and standard deviations of 0.02 and 0.01 s, respectively, and  
 449 the outliers are simulated by contaminating 1% of the P and S differential arrival times  
 450 with random noise generated from a uniform distribution between -0.2 and 0.2 s. We then  
 451 apply the preprocessing and robust slope estimation procedures to these data and com-  
 452 pare the estimated slopes with the input value (Fig. 12). The results show that in all  
 453 three cases, the estimated slopes perfectly match the input slope. We also perform the  
 454 same test on differential arrival times generated assuming a  $V_p/V_s$  ratio of 1.30, another  
 455 extreme value for rock s, which also shows a very good agreement between the estimated  
 456 and input slopes (Fig. S3). These tests demonstrate that the preprocessing procedure  
 457 does not bias the  $V_p/V_s$ -ratio estimates.

458 A common way to estimate the uncertainty of in-situ  $V_p/V_s$  ratios is the bootstrap-  
 459 resampling method (e.g., Lin & Shearer, 2007). This method quantifies the coherency  
 460 of a given set of differential arrival times. However, the uncertainty given by bootstrap  
 461 resampling is likely an underestimate because it does not account for the uncertainty as-  
 462 sociated with the data-selection procedure (Fig. 2). Therefore, in addition to bootstrap  
 463 resampling, we also performed sensitivity tests on  $N_{\min}$ ,  $RMS_{\max}$ , and  $\tau_{\min}$ , three key  
 464 parameters of the preprocessing procedure, to evaluate their effects on the  $V_p/V_s$ -ratio  
 465 estimates. The results show that the difference in  $V_p/V_s$  ratio between the barrier zone  
 466 and the mainshock zone is a robust feature regardless of parameter choice (Fig. 5).

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### 5.1.2 Uncertainty from Model Assumptions

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The in-situ  $V_p/V_s$ -ratio method implicitly assumes that the P and S waves from an event pair share the same ray path (Lin & Shearer, 2007), which is inaccurate in regions with strong 3D variations in  $V_p/V_s$  ratio. We thus used realistic 3D velocity models to evaluate their effects on the  $V_p/V_s$  ratio estimates (Figs. 8, 9, and S1). We showed that the  $V_p/V_s$ -ratio estimates of the fault zone can be biased towards the  $V_p/V_s$  ratio of the wall rock (smearing effects) and that the degree of bias depends on the width of the fault zone (Figs. 8, 9, and S1). Using event pairs with a smaller spatial separation could reduce the smearing effects and increase the spatial resolution. However, a small spatial separation would cause a narrower range of differential times and thus less reliable slope and intercept estimates (Fig. 4). Therefore, the choice of maximum inter-event separation likely controls the trade-off between estimation precision and accuracy. The synthetic tests also show that we can reliably resolve the relative difference in  $V_p/V_s$  ratio between different fault segments and time windows. The identified  $V_p/V_s$ -ratio contrast between the barrier zone and the mainshock zone likely exists, although the absolute value of the contrast may have been underestimated, similar to the conclusion of Bloch et al. (2018), which also used a comprehensive 3D synthetic test to verify their in-situ  $V_p/V_s$ -ratio observations.

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## 5.2 Comparison with Previous Tomography Results

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The tomography models of Guo et al. (2018) show a strong lateral variation in velocities in the G3 fault zone. The tomography models, including a  $V_p/V_s$ -ratio model, are obtained using the same OBS waveform data but a different earthquake catalog (Guo et al., 2018; Gong & Fan, 2022). The  $V_p/V_s$ -ratio model of Guo et al. (2018) suggests a greater range of  $V_p/V_s$ -ratio variation ( $\sim 1.5$ – $2.1$ ) than our results ( $\sim 1.6$ – $1.8$ ; Fig. S4). Both studies agree qualitatively on the high  $V_p/V_s$  ratio in F2 and the low  $V_p/V_s$  ratios in T, M1, and M2 (Fig. S4). In contrast, Guo et al. (2018) does not observe high  $V_p/V_s$  ratios in F1, D1, and D2 as shown by our results (Fig. S4). The comparison in E may not be meaningful because both models have lower resolutions in the region. The tomography model shows a high  $V_p/V_s$  ratio above  $\sim 4$  km depth in the distance ranges  $-30$ – $13$  km and  $\sim -7$ – $5$  km along strike, which are not resolved in our results (Fig. S4).

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The apparent differences between our results and those from Guo et al. (2018) may be due to the differences in sensitivity between our method and the tomographic-inversion approach used in Guo et al. (2018). Our method directly estimates the  $V_p/V_s$  ratio in a compact earthquake cluster by solving an over-determined problem of fitting a line to the differential arrival times, which is likely to yield a robust result. The small footprints of earthquake clusters also provide a high spatial resolution. In contrast, Guo et al. (2018) used differential arrival times to solve for the  $V_p/V_s$  ratios on a mesh of dense grid points in the volume occupied by their event pairs. Although such a method may offer a higher spatial resolution, the ill-conditioned problem requires smoothing and regularization to stabilize the inversion (Guo et al., 2018). The models of Guo et al. (2018) may provide constraints on the material properties of the shallow part of the barrier zone where earthquakes are sparse. The collective observations of both studies suggest an elevated  $V_p/V_s$  ratio in the entire barrier zone, consistent with sea-water infiltration down to the upper mantle in the barrier zone, causing the deep seismicity in D1 and D2 (McGuire et al., 2012).

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## 5.3 Physical State of G3 Fault Zone

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### 5.3.1 Fault-Zone Structural Complexity

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The percentage of the measurements passing the preprocessing procedure, defined as retention rate, may also offer information about the structural complexity in the fault

516 zone. In the CC step, D1 and D2 show a high retention rate of 40–50%; M1, M2, F1,  
 517 F2, and E show an intermediate retention rate of 15–35%; S1, S2, and T show a low re-  
 518 tention rate of <10% (markers with light-gray edges in Fig. 13). The linearity-step re-  
 519 tention rates generally correlate with the CC-step retention rates except for D1 and D2,  
 520 though the linearity-step retention rates are significantly lower (< 10%; markers with  
 521 dark-gray edges in Fig. 13). The retained events in F2 are mostly located in the deep  
 522 part of the patch (Fig. 1d), suggesting a possible difference between the shallow and deep  
 523 parts of F2. The data retention rate of the CC step is a proxy of the waveform similar-  
 524 ity between nearby events, which is analogous to the waveform similarity coefficient de-  
 525 fined in Trugman et al. (2020). The different data retention rates of different fault patches  
 526 might be caused by a variation in medium complexity, with a higher medium complex-  
 527 ity causing a higher waveform complexity, which results in cross-correlation results with  
 528 lower quality and thus a lower retention rate. Medium complexity includes both stress  
 529 and structural heterogeneity (e.g., material heterogeneity and fault networks), which are  
 530 closely related. Particularly, the low retention rate of F2 might be due to its high de-  
 531 gree of fracturing, especially in its shallow portion (Fig. 13), which could have enabled  
 532 hydrothermal circulation to produce a highly heterogeneous velocity structure. Such a  
 533 fluid-saturated fault zone could have strong dilatency effects, which could have been the  
 534 physical cause of the barrier zone repeatedly stopping the *M6* ruptures on the adjacent  
 535 fault segments (Liu et al., 2020).

### 536 5.3.2 Physical Models of Fluid-Saturated Rocks

537 Variations of  $V_p/V_s$  ratio in the oceanic lithosphere have long been associated with  
 538 the presence of pore fluids (e.g., Spudich & Orcutt, 1980; Barclay et al., 2001; Bloch et  
 539 al., 2018), and both fluid fraction and pore geometry were known to control the  $V_p/V_s$   
 540 ratios of water-saturated rocks (e.g., Shearer, 1988; Lin & Shearer, 2009). To investigate  
 541 the physical causes of the observed in-situ  $V_p/V_s$  ratios, we examine the effects of fluid  
 542 fraction and pore geometry by building idealized porous-medium models and compar-  
 543 ing their predictions with the observations. We assume an intact rock matrix with ran-  
 544 domly oriented spheroidal pores filled with water, which is characterized by the fluid vol-  
 545 ume fraction  $\phi$  ( $0 < \phi < 1$ ) and the aspect ratio of the spheroidal pores  $\epsilon$  ( $0 < \epsilon <$   
 546  $1$ ). For each combination of  $\phi$  and  $\epsilon$ , we follow Berryman (1980) to construct a self-consistent  
 547 model to compute the effective  $V_p/V_s$  ratio of the medium. Our model requires the elas-  
 548 tic parameters and densities of the rock matrix and water. For the rock matrix, we choose  
 549 two representative rock types for oceanic crust and upper mantle, namely diabase (Alt  
 550 et al., 1993) and harzburgite (Lippard, 1986). Their physical properties are adjusted to  
 551 a temperature and pressure condition of 600 °C and 150 MPa following Abers and Hacker  
 552 (2016) (hereafter, the physical properties mentioned are all for 600 °C and 150 MPa un-  
 553 less specified otherwise). We obtain the bulk modulus and density of high-temperature-  
 554 and-pressure water from the specific volume and entropy data in Tödheide (1972). The  
 555 physical properties of the rock matrices and water at the assumed temperature and pres-  
 556 sure are summarized in Table S2.

557 We compute the effective  $V_p/V_s$  ratios of porous rocks as functions of fluid volume  
 558 fraction in the range 0–0.1 assuming different pore aspect ratios for both diabase and  
 559 harzburgite (Fig. 14). The volume-fraction range is derived from Roland et al. (2012),  
 560 which suggests the barrier zone having a porosity of  $\sim 8\%$ . We find that in the case of  
 561 a small pore aspect ratio ( $\epsilon < 0.02$ ; thin cracks), the effective  $V_p/V_s$  ratio first decreases  
 562 then increases with increasing fluid volume fraction, whereas in the case of a large pore  
 563 aspect ratio ( $\epsilon > 0.02$ ; thick cracks), the effective  $V_p/V_s$  ratio decreases with increas-  
 564 ing fluid fraction (Fig. 14). Our results are consistent with the predictions of similar mod-  
 565 els from previous studies (e.g., Shearer, 1988). The effective  $V_p/V_s$  ratios of the diabase  
 566 model and the harzburgite model show the the same relation with fluid fraction and pore  
 567 aspect ratio except that the former is greater than the latter due to a greater  $V_p/V_s$  ratio  
 568 for intact diabase (1.81) than intact harzburgite (1.73; Fig. 14).

### 5.3.3 Comparison between In-situ $V_p/V_s$ Ratios and Physical-model Predictions

We compare the  $V_p/V_s$ -ratio estimates for F1, F2, M1, and M2 with the predictions of the diabase model because these patches are located in the crust and compare the estimates for D1 and D2 with the predictions of the harzburgite model because they are likely located in the upper mantle (Fig. 14). The  $V_p/V_s$ -ratio estimates of the fault patches fluctuated during the observation period (Figs. 6 and 7), which may reflect changes in fluid fraction and pore aspect ratio. We thus use the minimum and maximum  $V_p/V_s$ -ratio estimates as the reference values for each fault patch and compare them with the predictions of the physical models (Fig. 14). For F1 and F2, their minimum  $V_p/V_s$  ratios are close to the lower bound of all models and are only consistent with the model with  $\epsilon \approx 0.05$  and  $\phi \approx 0.08$ . The maximum  $V_p/V_s$  ratios of the two fault patches are close to the  $V_p/V_s$  ratio of intact diabase and can be explained with models with a wide range of  $\epsilon$  and  $\phi$  (Fig. 14a). Intriguingly, the  $V_p/V_s$ -ratio ranges of M1 and M2 are below the lower bound of all models (Fig. 14a). For the mantle patches, the minimum  $V_p/V_s$  ratios of D1 and D2 are consistent with a wide range of  $\phi$  and  $\epsilon$ , whereas their maximum values can only be explained by models with a high fluid volume fraction ( $\phi > 0.06$ ) and a small pore aspect ratio ( $\epsilon < 0.02$ ; Fig. 14b).

Our  $V_p/V_s$ -ratio estimates at G3 can generally be explained by porous-medium models with a reasonable fluid volume fraction, which are consistent with other geophysical evidence (Roland et al., 2012). However, the fluid volume fraction cannot be independently determined due to its coupled effects with pore geometry, which is largely unknown (e.g., pore aspect ratio; Fig. 14). Nonetheless, the fluid fraction and pore geometry of the G3 fault zone can be independently constrained by searching for parameter combinations that match both the  $V_p$  and  $V_p/V_s$  ratios or by incorporating electromagnetic observations, which are also sensitive to pore fluids. (e.g., Takei, 2002; Naif et al., 2015).

The porous-medium models show that the  $V_p/V_s$  ratios of M1 and M2 are too low to be caused by pore fluids alone and thus require other physical mechanisms (Fig. 14a). Thermal structure of oceanic transform faults varies gradually along strike (Roland et al., 2010) and thus is unlikely the cause of the sharp  $V_p/V_s$ -ratio contrast between the mainshock zone and the barrier zone (Fig. 1d). Furthermore, neither diabase nor harzburgite shows a significant change in  $V_p/V_s$  ratio within the possible temperature range (Fig. S5; Abers & Hacker, 2016). Chemical alteration may strongly affect the  $V_p/V_s$  ratio of the fault-zone materials. However, Roland et al. (2012) ruled out the presence of a significant amount of serpentine in the G3 barrier zone based on gravity measurements. Therefore, we speculate that other metamorphic minerals from reactions between the basaltic crustal rocks and sea water may have caused the low  $V_p/V_s$  ratios of M1 and M2. Specifically, low-grade metamorphic reactions could transfer anorthite in basaltic rocks into minerals with lower  $V_p/V_s$  ratios, such as zeolite (1.77), prehnite (1.73), and epidote (1.63) (Best, 2003). Such processes would systematically reduce the  $V_p/V_s$  ratios of M1 and M2, effectively shifting the curves in Fig. 14 downward, and the  $V_p/V_s$ -ratio estimates of M1 and M2 would be consistent with models with large pore aspect ratio (thick cracks; Fig. 14a). In this case, the sharp contrast in  $V_p/V_s$  ratio between the mainshock zone and the barrier zone (Fig. 1d) could be due to a combined effect of pore fluids and chemical alteration. These inferences of fault-zone material properties will benefit from further petrological and petrophysical investigations on the materials in the Gofar fault zone.

The temporal evolution of the  $V_p/V_s$  ratios in F1, F2, D1 and D2 within a few months before the mainshock is unlikely due to a change in mineral composition because metamorphic reactions occur much more slowly (Figs. 6c-f). Therefore, these temporal changes in  $V_p/V_s$  ratio are likely due to perturbations of pore fluids. The idealized porous-medium models suggest that a decrease in pore aspect ratio (i.e. thick cracks transitioning into thin cracks) and an increase in fluid fraction can cause an increase in  $V_p/V_s$ -ratio, which may explain the nine-month  $V_p/V_s$ -ratio increase observed for F1, F2, D1, and D2 (Fig. 14).

Fluid migration can affect both fluid fraction and pore aspect ratio while causing seismic and aseismic slips (Huang et al., 2019; Ross et al., 2020). Besides, shear sliding can alter pore spaces via dilatancy effects (Liu et al., 2020), which may couple with fluid migration to influence the  $V_p/V_s$  ratios in the fault zone. Our findings suggest that in-situ  $V_p/V_s$  ratios can be used to monitor the physical state of fault-zone materials at great spatial and temporal resolutions.

## 6 Conclusions

We develop a new method to compute in-situ  $V_p/V_s$  ratios using differential arrival times of nearby earthquakes. We apply this method to ocean-bottom-seismometer data at the westernmost Gofar transform fault and find that the fault zone material has a robust along-strike variation in  $V_p/V_s$  ratio, with the eastern segment, which includes the barrier zone, having a moderate  $V_p/V_s$  ratio of 1.75–1.80 and the western segment, which includes the down-dip edge of the 2008 *M*6 earthquake, having a low  $V_p/V_s$  ratio of 1.61–1.69. This variation may be caused by differences in pore fluids and chemical alteration. We also observe a nine-month  $V_p/V_s$ -ratio increase in the barrier zone, which may be caused by a combined effect of an increasing number of thin cracks and increasing fluid fraction. Our results suggest that the in-situ  $V_p/V_s$ -ratio method is a useful tool for monitoring the physical state of fault-zone materials.

## 7 Open Research

The waveform data are downloaded from the Data Management Center (DMC) of the Incorporated Research Institutions for Seismology (IRIS) under the network codes ZD. The metadata of the network can be accessed at <https://ds.iris.edu/mda/ZD/?starttime=2007-01-01T00:00:00&endtime=2009-12-31T23:59:59>. The earthquake catalog is from Gong and Fan (2022) (DOI:10.1002/essoar.10511753.1). The bathymetry data are obtained from <https://www.ngdc.noaa.gov/maps/autogrid/>. The SciPy TLS package is described at <https://docs.scipy.org/doc/scipy/reference/odr.html>. Pykonal is available at <https://github.com/malcolmw/pykonal>.

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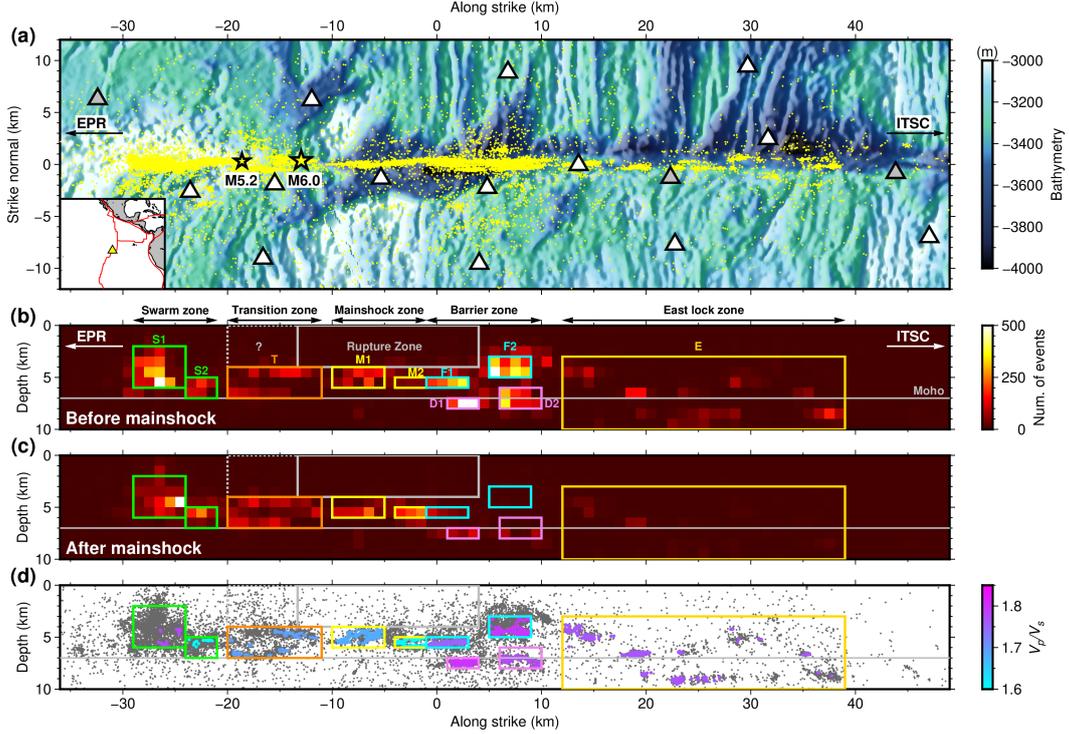
T.L. is supported by National Science Foundation (NSF) grants EAR 1829601 and EAR 2123529 and a Green Postdoctoral Scholarship. J.G. and W.F. are supported by NSF grants OCE-1833279 and EAR-2143413. G.L. is supported by EAR-2022429. The ocean bottom seismometer instruments were provided by the Ocean Bottom Seismograph Instrument Center (OBSIP). We thank Malcolm White for helping us use PyKonal and Geoffrey Abers for helping us calculate physical properties of rocks at high temperatures and pressures. We thank Hao Guo for sharing the data file of the model in his paper. We thank Jeffrey McGuire, John Collins, and the rest of the 2008 Quebrada-Discovery-Gofar experiment team for collecting and archiving the data. IRIS Data Services are funded through the Seismological Facilities for the Advancement of Geoscience and EarthScope (SAGE) Proposal of the National Science Foundation (NSF) under Cooperative Agreement EAR-1261681.

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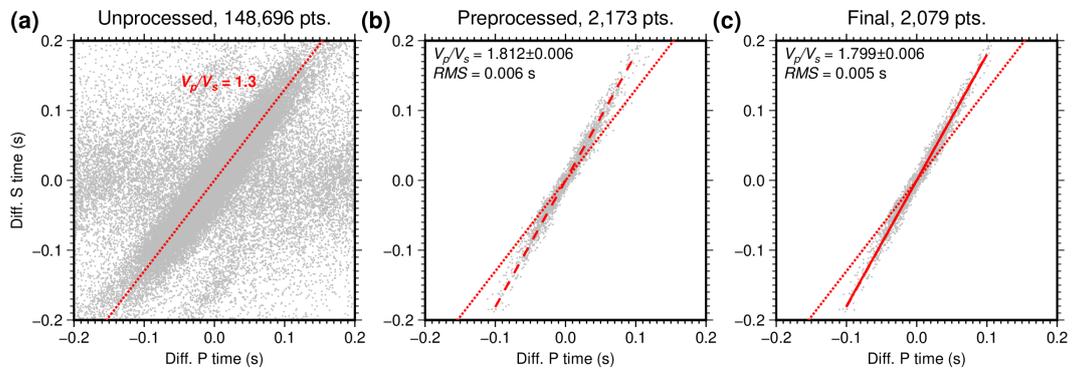
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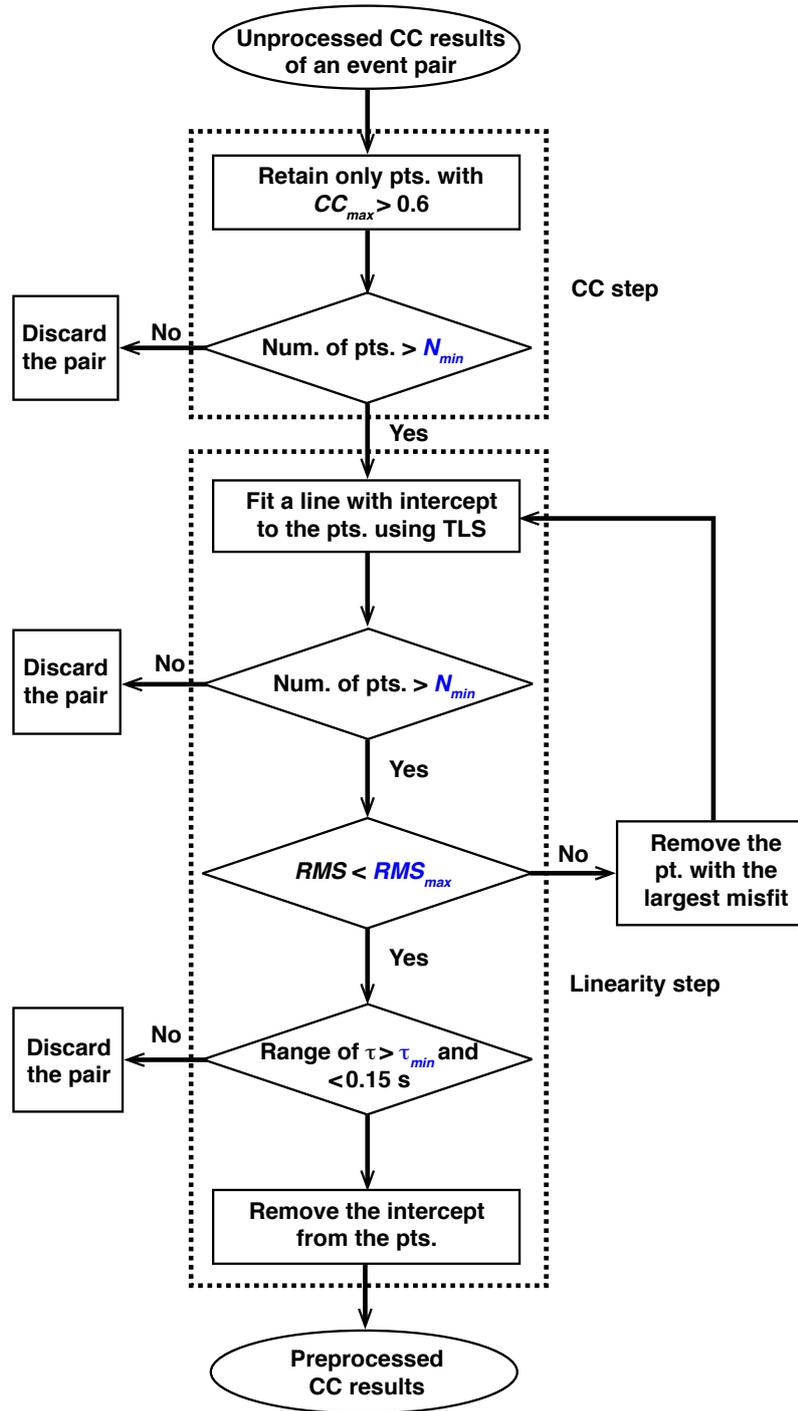
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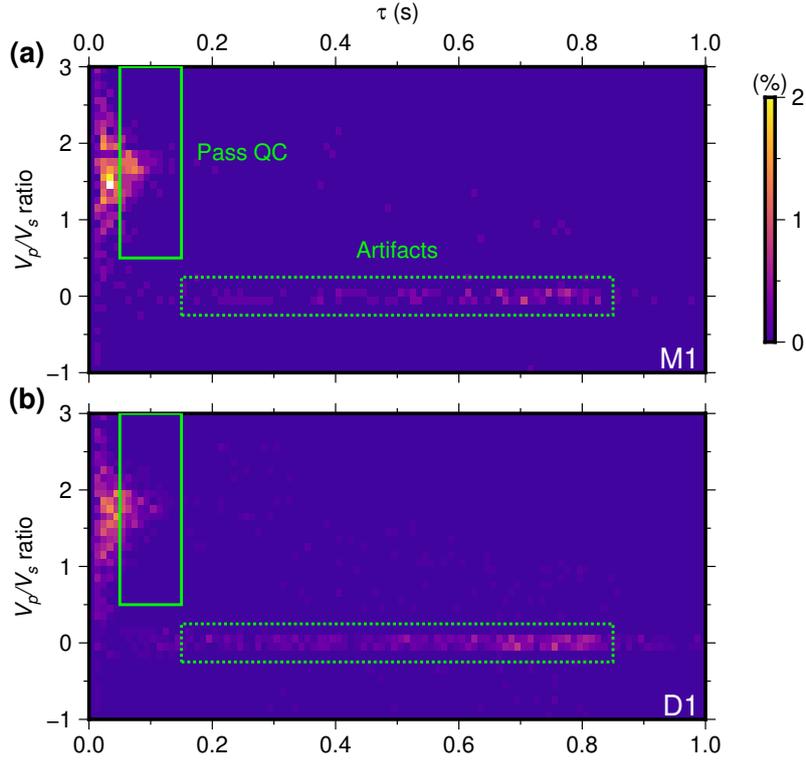
**Figure 1.** Summary of the observation geometry and the  $V_p/V_s$ -ratio estimates of each fault patch. The origin of the along-strike axis is approximately the same as the one in Figure 3 of McGuire et al. (2012). (a) Stations (triangles; functional and non-functional ones in white and gray, respectively) and events (yellow dots) plotted on the bathymetry of G3. Big and small stars: The  $M6.0$  mainshock and the largest aftershock of  $M5.2$ . The East Pacific Rise (EPR) and an intra-transform spreading center (ITSC) are immediately west and east of the map boundaries, respectively. Inset: A regional map of the east Pacific showing the location of G3 (yellow triangle) and the plate boundaries (red lines). (b) Seismicity density on the fault plane before the mainshock, binned with  $1\text{ km} \times 1\text{ km}$  grids. Rectangles with different colors mark different fault patches. Dashed gray rectangle: possible  $M6$  rupture in the transition zone. (c) Similar to (b), but for the events after the mainshock. (d) Average  $V_p/V_s$  ratios of all fault patches. Gray dots: All events in Gong and Fan (2022). Colored dots: Events used for estimating the  $V_p/V_s$ -ratios, colored by the  $V_p/V_s$  ratios of the corresponding fault areas.



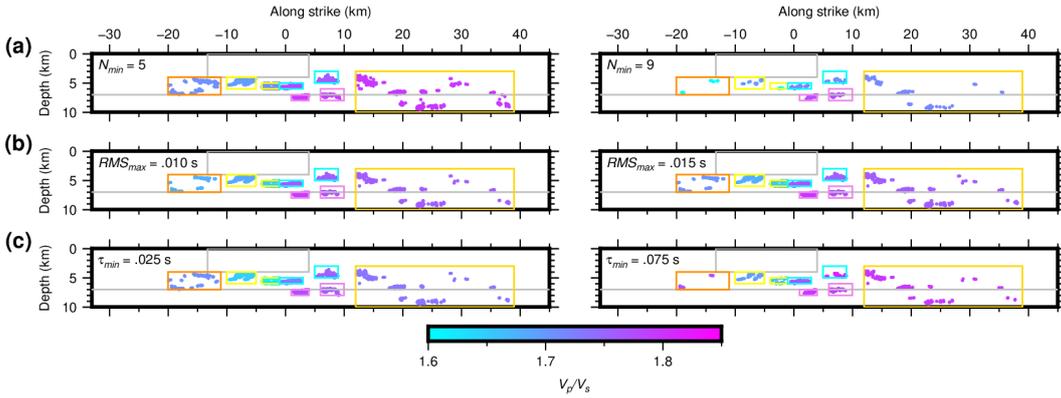
**Figure 2.** Differential P and S arrival times of the fault area D1 (Fig. 1b, c, and d) at three data-processing steps. Dotted red lines: Reference line with a slope of 1.3. Dashed red line: Line with a slope equal to the  $V_p/V_s$  ratio estimated using all preprocessed measurements. Solid red line: Line with a slope equal to the final estimated  $V_p/V_s$  ratio. (a) Unprocessed differential arrival times. (b) Differential arrival times after preprocessing. (c) Differential arrival times used for the final  $V_p/V_s$ -ratio estimation.



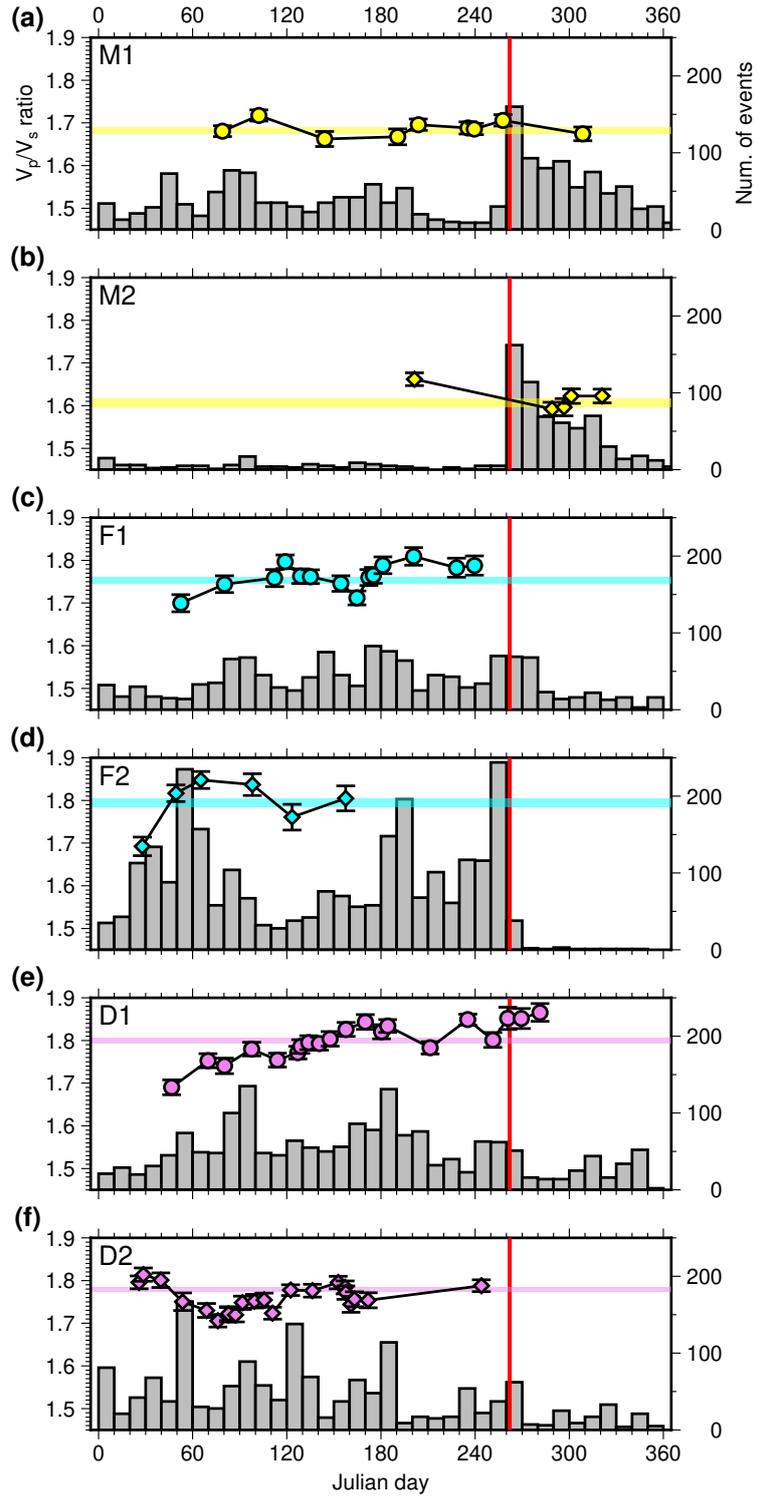
**Figure 3.** Summary of the preprocessing workflow. The key parameters tested in 5 are blue.



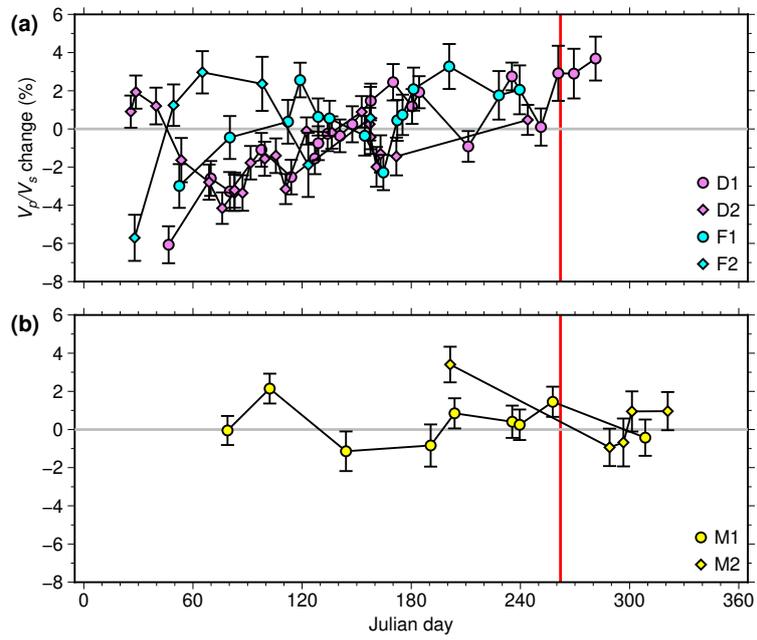
**Figure 4.** Joint distributions between the  $V_p/V_s$  ratios and differential-P-time ranges ( $\tau$ ) of the event pairs with intercept terms removed for (a) M1 and (b) D1. Solid green box: The preferred range of measurements for  $V_p/V_s$  ratio (0.5–3) and  $\tau$  (0.05–0.15 s). Dotted green box: A cluster likely consisting of artifacts.



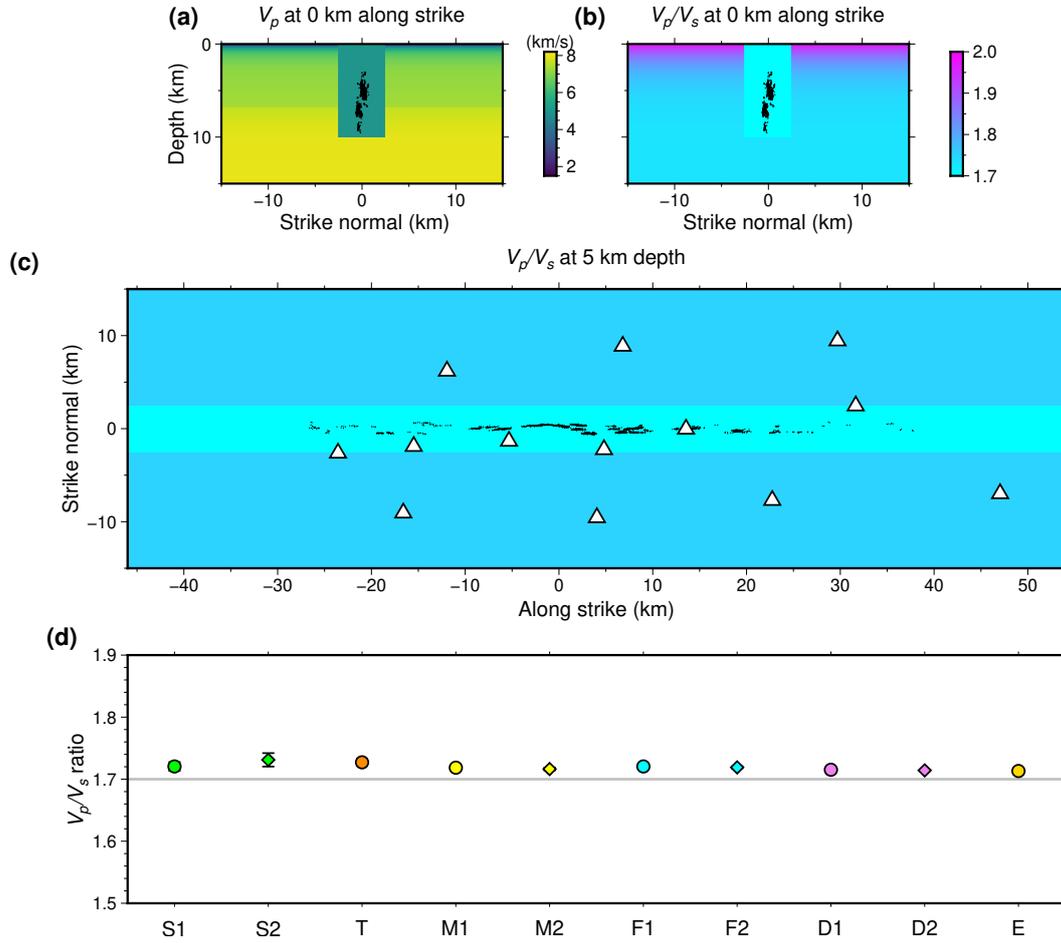
**Figure 5.** Effects of the three key preprocessing parameters  $N_{\min}$ ,  $RMS_{\max}$ , and  $\tau_{\min}$  on the spatial pattern of the estimated  $V_p/V_s$  ratios. The two columns show the results of two alternate choices for (a)  $N_{\min}$  (5 and 9), (b)  $RMS_{\max}$  (0.010 and 0.015 s), and (c)  $\tau_{\min}$  (0.025 and 0.075 s) in comparison with the results of the preferred parameter choice shown in Fig. 1d. Colored dots and boxes are the same as the ones in Fig. 1d.



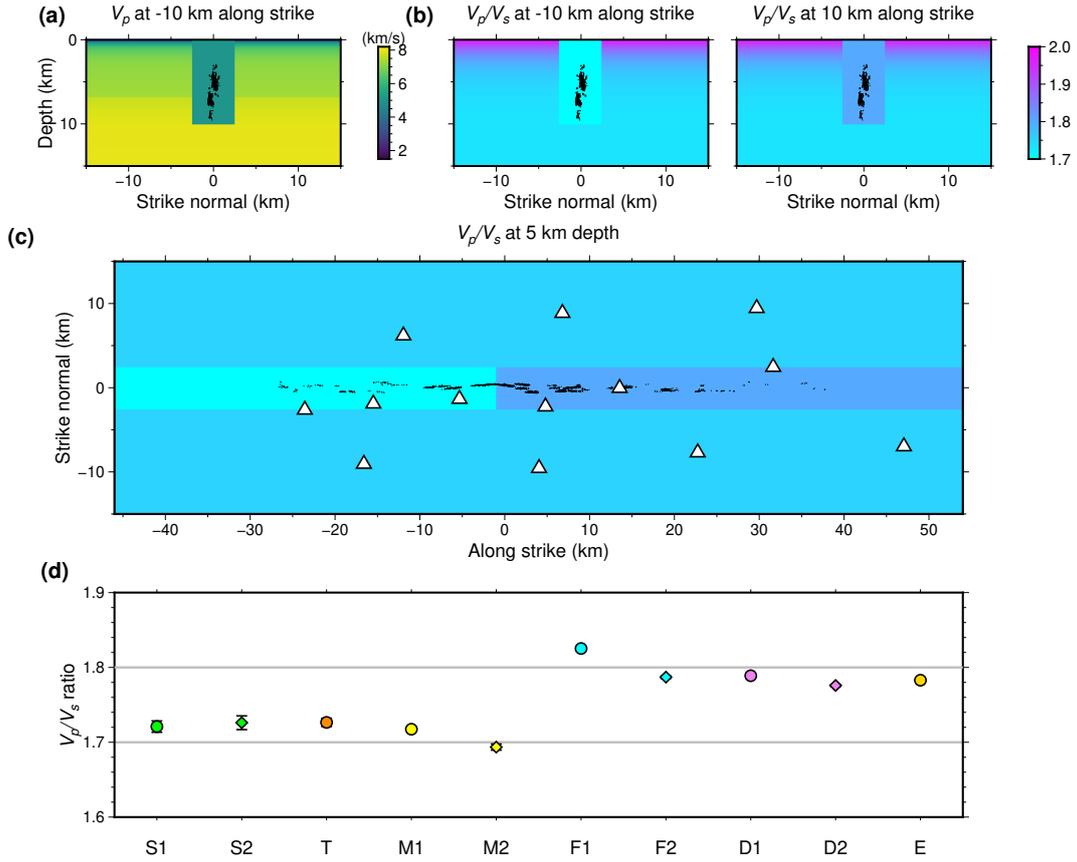
**Figure 6.** Temporal variations of the in-situ  $V_p/V_s$  ratios of (a) M1, (b) M2, (c) F1, (d) F2, (e) D1, and (f) D2. Colored markers:  $V_p/V_s$  ratio of each time window plotted at the center of the window. Colored bands: Uncertainty ranges of the temporal average  $V_p/V_s$  ratios. Gray histograms: Event counts with a 10-day bin width. Red vertical line: Time of the mainshock.



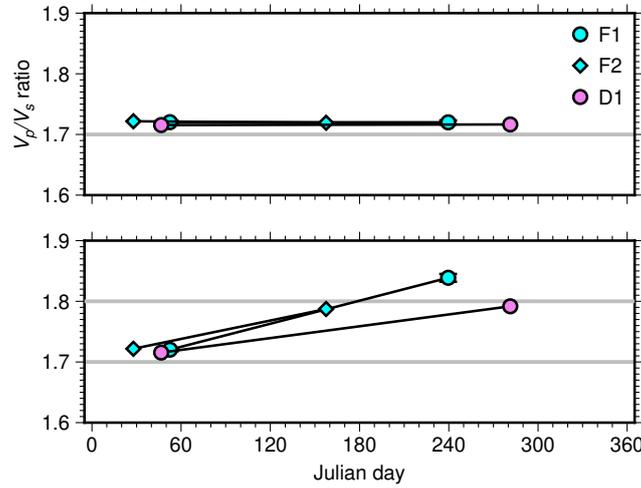
**Figure 7.** Percentage changes of the  $V_p/V_s$  ratios of (a) F1, F2, D1, and D2 and (b) M1 and M2. The changes are relative to the average  $V_p/V_s$  ratios of the respective fault patches.



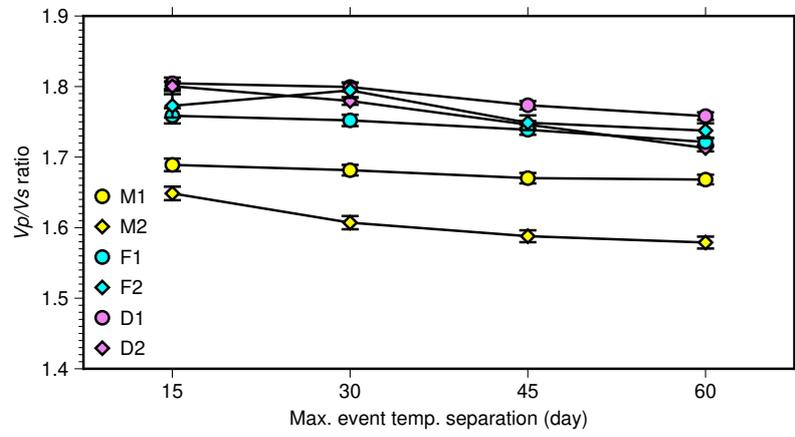
**Figure 8.** Summary of the 3D synthetic test assuming a homogeneous fault zone (Model 1). Black dots: Events used for the final  $V_p/V_s$ -ratio estimation. White triangles: Functional stations in 1a (a) Cross section of the  $V_p$  model at 0 km along strike. (b) Cross section of the  $V_p/V_s$  model at 0 km along strike. (c) Cross section of the  $V_p/V_s$  model at the depth of 5 km. (d) Retrieved  $V_p/V_s$  ratios of all fault patches (colored markers) compared with the input  $V_p/V_s$  ratio of the fault zone (gray line).



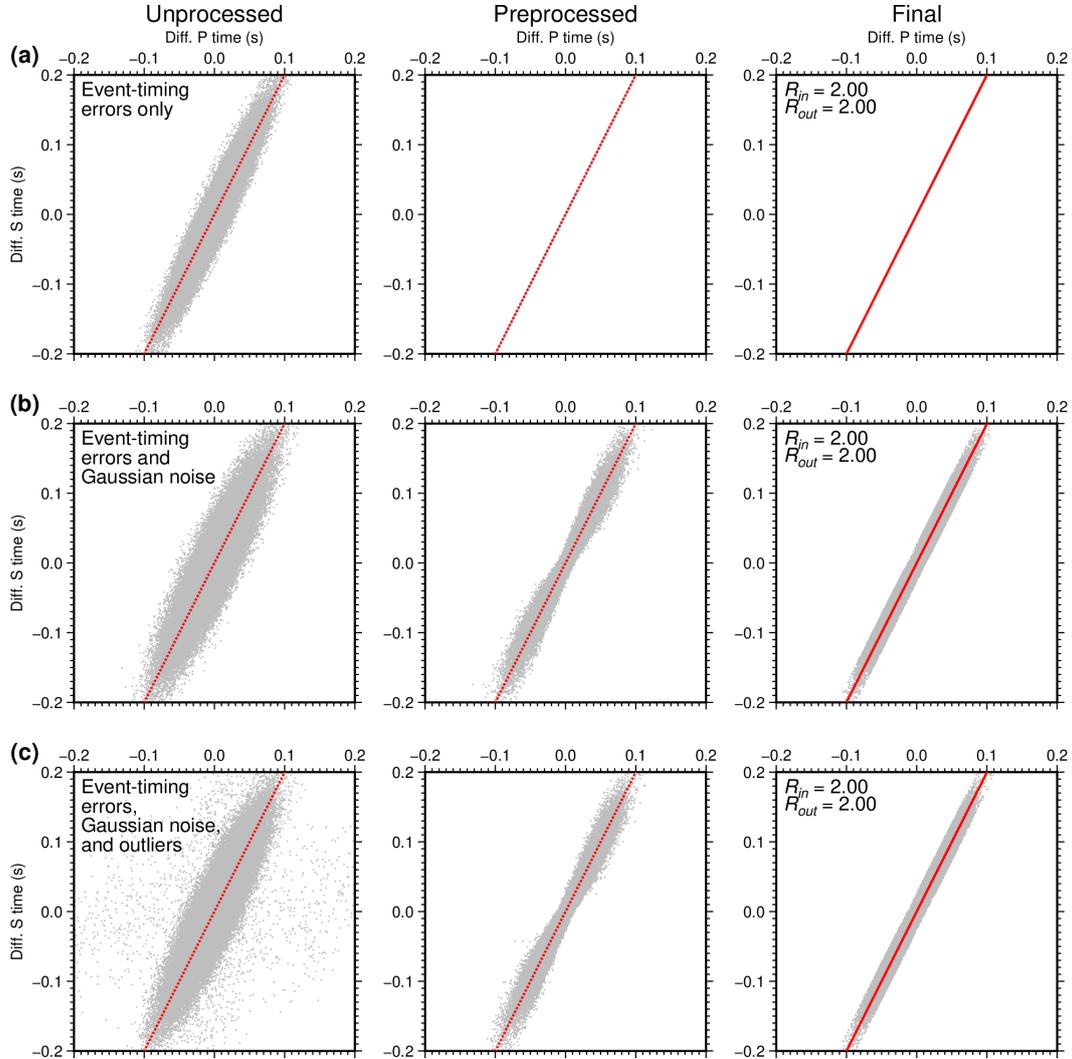
**Figure 9.** Similar to Fig. 8, but for the model with a segmented fault zone (Model 2). The gray lines in (d) mark the input  $V_p/V_s$  ratios of the two segments.



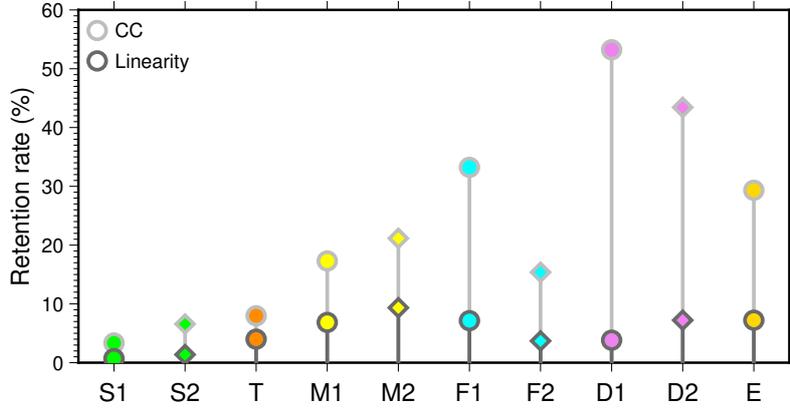
**Figure 10.** Synthetic tests of the temporal  $V_p/V_s$ -ratio increase in F1, F2, and D1. (a) Results for the case with Model 1 as the velocity model at both the first and second time windows. Colored markers:  $V_p/V_s$ -ratio estimates for the first and second time windows of the three patches of interest. Gray line: Input fault-zone  $V_p/V_s$  ratio. (b) Similar to (a) but for the case with Model 1 at the first window and Model 2 at the second window. Gray lines: Input fault-zone  $V_p/V_s$  ratios for the two time windows.



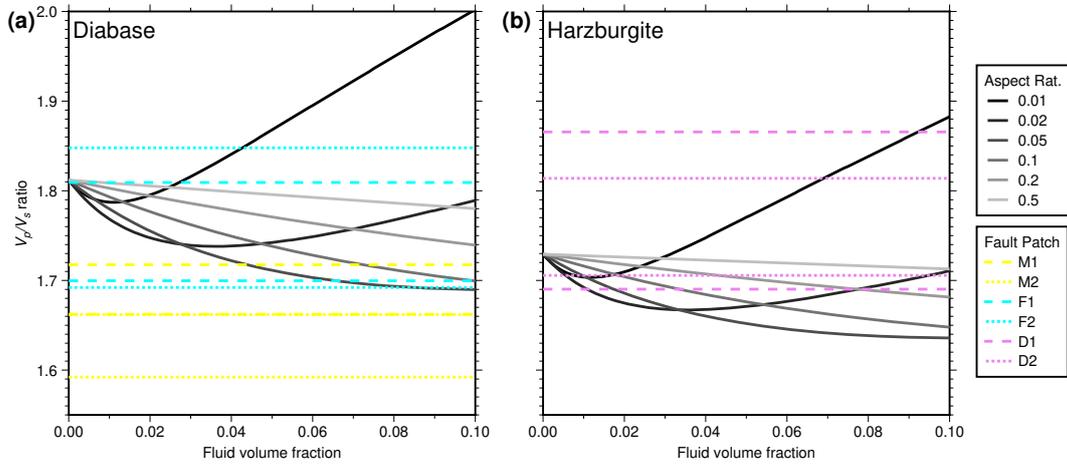
**Figure 11.** Effects of maximum temporal separation of event pairs on the  $V_p/V_s$ -ratio estimates for six fault patches. Colored markers:  $V_p/V_s$  ratios of different fault patches.



**Figure 12.** Synthetic tests of the effects of the preprocessing and robust-slope-estimation procedures. Dotted and solid red lines: Slope of the input noise-free data (2.00) and the slopes obtained from the estimation procedure, respectively. The three columns from left to right show input data points, the remaining data points after preprocessing, and the data points used for the final slope estimation, respectively. (a) Case with only event-timing errors. (b) Case with event-timing errors and Gaussian noise. (c) Case with event-timing errors, Gaussian noise, and outliers.



**Figure 13.** Data retention rates for all fault patches. The rates for the cross-correlation-value (CC) step and the linearity step are outlined in light and dark gray, respectively.



**Figure 14.** Physical models of effective  $V_p/V_s$  ratios of porous rocks for a rock matrix of (a) diabase (Alt et al., 1993) and (b) harzburgite. (Lippard, 1986). Black to light-gray curves: Models colored by their pore aspect ratios. Colored dashed and dotted lines: Ranges of the  $V_p/V_s$  ratio estimates for the six patches in the mainshock zone (M1 and M2) and the barrier zone (F1, F2, D1, and D2).