

Supporting Information for ”Subsurface Mixing Dynamics across the Salt-freshwater Interface”

K.De Vriendt¹, T.Le Borgne², M.Pool³, M.Dentz¹

¹IDAEEA-CSIC, Institute of Environmental Assessment and Water Research, Spanish National Research Institute

²Universit de Rennes 1, CNRS, Goscience Rennes UMR 6118, Rennes, France

³AMPHOS 21 Consulting S. L., 08019 Barcelona

¹18 26, Calle Jordi Girona, 18-26, 08034 Barcelona

1. Model Parameters

Values of parameters used in the numerical simulations are provided in table S1.

1.1. Dispersivities

Numerical studies have shown that the longitudinal and transverse dispersivities α_l and α_t are important parameters when considering mixing dynamics and the width of the SFI (e.g. Abarca et al., 2007; Nick et al., 2013; Spiteri et al., 2008). Unlike the evolution of plumes over time, there exists no clear criterion for assigning the value of dispersivities (Rezaei et al., 2005). This is further confounded by the fact that it is a parameter that is generally difficult to measure and is scale dependent (Neuman, 1990). Numerical

studies of field sites often adopt arbitrarily large dispersivity values in order to overcome numerical dispersion caused by poor grid refinement in numerical codes (Paster, 2010), or to artificially incorporate the effects of tides and heterogeneity (Werner et al., 2012). However, large dispersion likely lead to an overestimation of mixing induced reaction rates.

In Figure S2, we see that increasing α_l has negligible impact on the overall mixing width compared to α_t . For example, increasing α_l by a factor of 5 for $\alpha_t = 0.01$ m, results in almost no change in s_m . This is not surprising given the bulk of the interface resides where flow is tangential to the principal direction of flow. Flow from the seaside however approaches the interface orthogonally with velocities approximately an order of magnitude lower than the freshwater flux. This, however is by no means suggesting α_l play no role in the behaviour of the mixing zone. Abarca et al. (2007) showed that increasing α_l leads to the seaward displacement of high concentration isolines, with a particularly strong influence at toe. Therefore for larger values of α_l , the analytical solution may no longer provide a good fit. For smaller dispersivities however, which are in-line with literature values seen in table S2, α_t alone seems to sufficiently characterizes the growth of s .

2. Mixing width

To determine the mixing width, we compute the distance across $c(1 - c)$ at half its maximum, denoted here as κ . Due to the proximity of the toe to boundary, the full width at half maximum cannot be attained directly at the bottom and are omitted. For a symmetric profile of $c(1 - c)$, we can relate this back to the square root of the second central moment (variance) of $c(1 - c)$,

$$s = \frac{\kappa}{2\sqrt{2 \ln 2}}, \quad (1)$$

where s defines the mixing width.

3. Interface width and interface height

We first recall that the stretching rate is defined by

$$\gamma(z) = \frac{dv(z)}{dz}. \quad (2)$$

Inserting this expression into expression (8) in the main text for $s(z)$, we can write

$$s(z) = \sqrt{\alpha_t \left[\frac{d \ln v(z)}{dz} \right]^{-1}}. \quad (3)$$

We estimate the velocity along the interface from volume conservation and set

$$v(z) = \frac{q_f b}{\xi(z)}, \quad (4)$$

where $\xi(z)$ is the interface height that is $\xi(z=0) = b$ at the toe position at $z=0$ and 0 at the outflow. With this definition, we obtain for the interface width in Eq. (3)

$$s(z) = \sqrt{-\alpha_t \left[\frac{d \ln \xi(z)}{dz} \right]^{-1}}. \quad (5)$$

4. Interface width from the Glover solution

To derive an approximation for the mixing width in the compression regime, we consider the sharp interface solution of Glover (1959) that predicts the position of the interface as,

$$\xi^2 = \frac{2Q_f}{K\epsilon'} z + \frac{Q_f^2}{K^2\epsilon'^2}, \quad (6)$$

where $Q_f = q_f b$, recalling q_f is the freshwater flux and b is the domain height. To account for the influence of mixing we incorporate the empirical correction factor for the buoyancy

factor, ϵ' , as introduced by Pool (2011),

$$\epsilon = \epsilon' \left[1 - \left(\frac{\alpha_t}{b} \right)^{1/4} \right]^{-1}. \quad (7)$$

We implement the factor $1/4$ suggested by (Lu & Werner, 2013) as it provides a better fit against the numerical simulations. We transform equation (6) such that $z = 0$ coincides with the toe position. Thus, we obtain

$$\xi = \sqrt{b^2 - \frac{2b}{\text{Ng}' } z}, \quad (8)$$

where we defined the modified gravity number, $\text{Ng}' = K\epsilon/q_f$. Note that $\xi(z = 0) = b$.

The the length of the toe is predicted by the Glover solution as

$$L_t = \frac{b\text{Ng}'}{2}. \quad (9)$$

Inserting (8) into (5), we obtain for the interface width during the compression regime the explicit expression

$$s(z) = \sqrt{\alpha_t(\text{Ng}'b - 2z)}. \quad (10)$$

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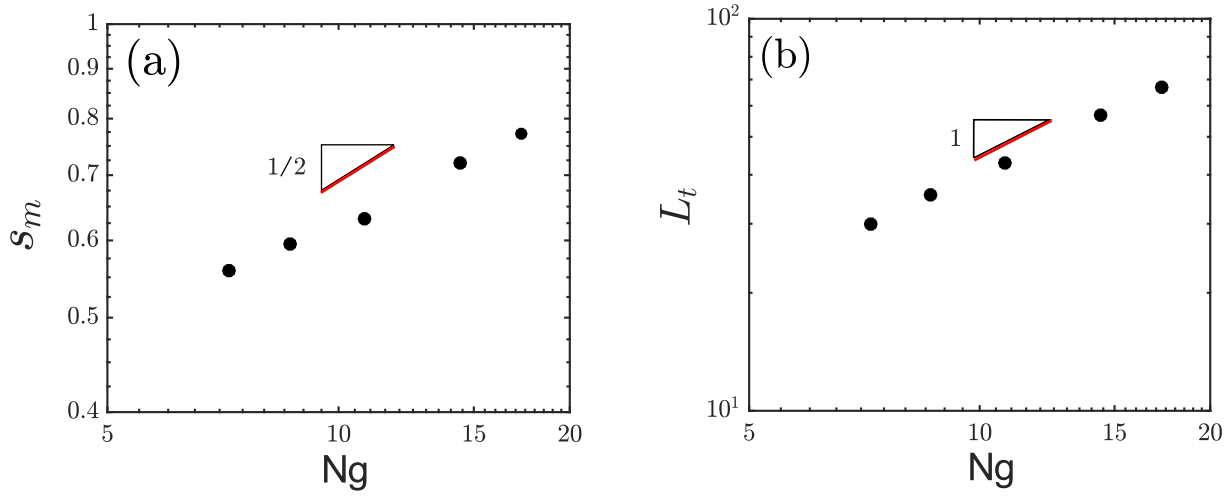


Figure S1. a) Maximum mixing width, s_m and the b) toe length, L_t obtained from numerical models as a function of Ng

Table S1. Parameters used in numerical simulations

Parameter	Value	Description
$K[ms^{-1}]$	1×10^{-4}	Hydraulic conductivity
$b[m]$	10	Aquifer thickness
$L[m]$	100	Aquifer Length
$\phi[-]$	0.3	Porosity
$\alpha_l[m]$	0.2	Longitudinal dispersivity
$\alpha_t[m]$	0.02	Transverse dispersivity
$q_f[md^{-1}]$	0.0125, 0.015, 0.02, 0.025 and 0.03	Freshwater flux
$Ng[-]$	17.3, 14.4, 10.8, 8.6 and 7.2	Freshwater flux
$D_m [m^2/s]$	$1e-9$	Molecular diffusion
$\epsilon'[-]$	0.025	Buoyancy factor

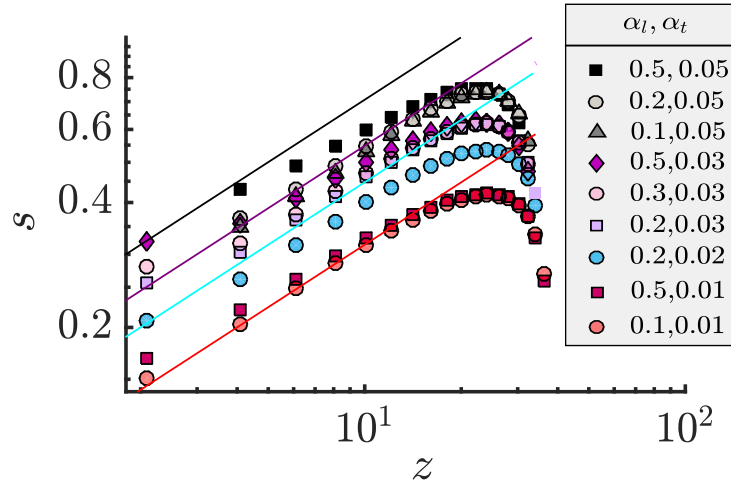
**Figure S2.** Mixing width for varying dispersivities. Solid lines indicate interface growth for the numerical transverse dispersivity.

Table S2. Literature derived values of coastal aquifer properties

Publication	Type	K [m/s]	q_f [m/d]	b [m]	α_l (m)	α_t (m)
Paster (2010)	Field	1.73×10^{-3}	-	600-1000	-	0.04
Abarca et al. (2013)	Field	1.74×10^{-4}	2.3×10^{-2}	11	0.1	0.01
Heiss and Michael (2014)	Field	2.9×10^{-4}	-	12-18	0.15	1.5×10^{-2}
Spiteri et al. (2008)	Field	6.86×10^{-4}	0.13	11	0.5	5×10^{-3}
C. Robinson et al. (2007)	Field	1.16×10^{-4}	6.6×10^{-2}	30	0.5	5×10^{-2}
Abarca and Clement (2009)	Experimental	1.2×10^{-2}	-	0.3	5×10^{-4}	5×10^{-5}
G. Robinson et al. (2015)	Experimental	2.3×10^{-3}	-	0.14	1×10^{-3}	5×10^{-4}
Masahiro et al. (2018)	Experimental	-	-	0.25	7×10^{-4}	2.5×10^{-5}

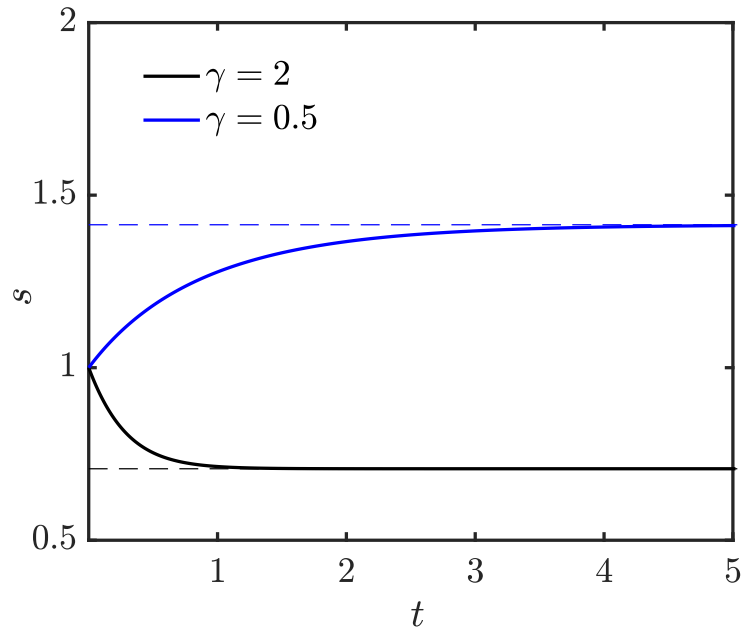


Figure S3. Evolution of mixing width given two different stretching rates. Blue line shows diffusive growth of an interface towards a large batchelor scale (blue dashed line) given a small stretching rate whereas the black line shows the mixing width compressing exponentially towards a small Batchelor scale (black dashed line)