

1 **Hazard assessment for typhoon-induced coastal flooding and inundation in Shanghai, China**

2

3 Jie Yin^{1,2,3}, Ning Lin^{2*}, Yuhan Yang¹, William J. Pringle⁴, Joannes J. Westerink⁴, Dapeng Yu⁵

4

5 1 Key Laboratory of Geographic Information Science (Ministry of Education), East China Normal University,

6 China

7 2 Department of Civil and Environmental Engineering, Princeton University, USA

8 3 Institute of Eco-Chongming, East China Normal University, China

9 4 Department of Civil and Environmental Engineering and Earth Sciences, University of Notre Dame, IN, USA

10 5 Department of Geography, Loughborough University, UK

11 * Correspondence to: N.L. (email: nlin@princeton.edu)

12

13 **Abstract:** This paper describes an integrated statistical-hydrodynamic method to estimate tropical cyclone-
14 induced coastal flood inundation hazard, applied to a coastal megacity-Shanghai, China. We identify three
15 “worst-case” scenarios (extracted from over 5000 synthetic storms) that generate unprecedentedly high flood
16 levels in Shanghai. Nevertheless, we find that the mainland Shanghai is relatively safe from coastal flooding
17 under the current climate, thanks to its high-standard seawall protection. However, the city is expected to be
18 increasingly at risk due to future sea level rise, with inundation two times and 20 times more likely to occur
19 by mid- and late-21st century, respectively, and inundation depth and area to greatly increase (e.g., 60-1360%
20 increase in the inundation area for the “worst cases” by 2100). The low-lying and poorly-protected area (e.g.
21 Chongming island) is likely to be moderately affected by flood events with long return periods at the current
22 state but could be largely inundated in future sea-level-rise situations.

23

24 **Key Points:**

- 25 1. An integrated statistical-hydrodynamic method is developed to estimate tropical cyclone-induced
26 coastal flood inundation hazard.
- 27 2. The mainland Shanghai is found to be well protected by high-standard seawalls.
- 28 3. However, Shanghai is expected to be increasingly at risk due to future sea level rise.

29

30 **Key Words:** Topical Cyclone, Storm Tide, Inundation, Sea Level Rise, Flood Protection, Shanghai

31

32 **Plain Language Summary:** Coastal flooding associated with tropical cyclones (TCs, also called typhoons in
33 the Northwest Pacific Basin) is often the most devastating and costliest of natural hazards. Struck by a number
34 of strong TCs in recorded history, Shanghai may be highly vulnerable to coastal flooding due to its location
35 within the Yangtze River delta, low-relief topography and high-density population. However, given the limited
36 historical data, observation-based analysis is insufficient to capture the potential extreme events. In this study,
37 we use a synthetic storm model to generate large numbers of TC events that are physically plausible but may
38 have never occurred in the past. Storm tide and the resultant coastal flooding induced by each TC are further
39 simulated with a coupled circulation-inundation model. Results suggest that Shanghai may encounter extreme
40 storm tide flooding with very low possibilities under the current climate condition. With the protection of
41 seawall, the city is generally immune to extensive flooding, except the low-lying and poorly-protected coastal
42 floodplain and estuarine island, Chongming. However, future sea level rise will induce a significantly
43 increased flood risk in Shanghai over the 21st century.

44

45 **1. Introduction**

46

47 Tropical cyclones (TCs), associated with extreme wind, rainfall and storm surge, are responsible for
48 significant property damage and loss of life in coastal areas ([Smith and Katz, 2013](#)). Often, TC-induced storm
49 surge together with astronomical high tide have been suggested as the primary causes of episodic flooding in
50 low-lying coastal regions. Recent flood catastrophes illustrate that coastal cities, as the agglomeration of
51 population and assets, are particularly vulnerable to storm tide flooding. For example, the unprecedented
52 flooding of New Orleans due to Hurricane Katrina (2005) caused hundreds of fatalities and more than \$40
53 billion in economic losses, making it the worst natural disaster in U.S. history ([Kates et al., 2006](#)). Hurricane
54 Sandy (2012) resulted in the deaths of tens of people due to drowning and at least \$20 billion in flood-related
55 damages in New York City ([Blake et al., 2013](#)). Coastal flooding is expected to be more frequent and
56 devastating, owing to rapid urbanization, sea level rise (SLR) and TC intensification in a warming climate
57 ([Emanuel, 2013](#); [Woodruff et al., 2013](#); [Hallegatte et al., 2013](#); [Lin and Shullman 2017](#); [Vitousek et al., 2017](#);
58 [Marsooli et al. 2019](#); [Knutson et al., 2020](#)). Hence, it is essential to quantify TC-induced flood hazards at city
59 or regional scales.

60

61 To ensure an accurate assessment of TC-induced flood hazards for coastal cities, a large number of TC events
62 are required particularly for addressing extreme flood hazards induced by low-probability storms. Due to the
63 lack of sufficient measurements over a long period, statistical methods have been commonly used to generate
64 large samples of synthetic TCs for a specific site (e.g., a city) of interest ([Batts et al., 1980](#); [Georgiou et al.,
65 1983](#)). The basic idea of these models is that probability distributions of key TC parameters (e.g., central
66 pressure and radius of maximum wind) are fitted to the historical record, and then a Monte Carlo approach is
67 applied to sample from these distributions. To overcome the limitation of local data, [Vickery et al. \(2000,
68 2009\)](#) applied the basin-wide data to develop a probabilistic track model with TC intensity along the track

69 estimated based on storm persistent and environmental variables such as the sea surface temperature.
70 Furthermore, Emanuel et al. (2008), Lee et al. (2018), and Jing and Lin (2020) developed more advanced
71 probabilistic track models by incorporating more environmental and oceanic variables that are essential to
72 storm development. The advent of synthetic TC simulation has enabled probabilistic TC hazard assessment
73 for coastal cities.

74

75 Recently, synthetic TC simulation has been increasingly used to drive storm tide simulation and assess flood
76 hazards at the city scale. Lin et al. (2010, 2012, 2016) applied the statistical-deterministic model developed by
77 Emanuel et al. (2008) to produce large numbers of synthetic storms for New York City (NYC), and then they
78 used two hydrodynamic models: the Sea, Lake and Overland Surges from Hurricanes (SLOSH) model
79 (Jelesnianski et al., 1992) and the Advanced Circulation (ADCIRC) model (Luettich et al., 1992; Westerink et
80 al., 1994) with a high resolution mesh (up to 10 m around NYC) to simulate storm surges and storm tides
81 induced by synthetic TCs. They estimated the probabilistic distribution of storm tides along NYC coast and
82 found a heavy tail for very low occurrence probability events. Furthermore, the simulated surge heights along
83 the coast from Lin et al. (2012) were interpolated and applied to terrain elevation for determining the flood
84 inundation (extent and depth) and associated probabilities for NYC (Aerts et al., 2013). However, the simple
85 nearest neighbor extrapolation method used in this analysis does not consider the dynamic nature of flood
86 routing and may cause biases in the final inundation maps (Barnard et al., 2019). More recently, Yin et al.
87 (2016) described a new method for coastal flood simulation by coupling ADCIRC and a simplified 2D flood
88 inundation model (FloodMap) and applied the analysis to NYC for the case of Hurricane Sandy. The coupled
89 model demonstrated efficiency and improved prediction over ADCIRC-only simulations for estimating storm-
90 induced flooding in coastal areas.

91

92 In this study, an integrated statistical-hydrodynamic approach is proposed by running the statistical-
93 deterministic hurricane model, ADCIRC, and FloodMap in sequence, to derive probabilistic flood hazard
94 maps and to investigate possible worst-case flood scenarios for coastal cities under the current climate
95 conditions as well as projected future SLR scenarios. To our knowledge, this study is the first that couples
96 probabilistic hurricane model, storm surge model, inundation model, coastal protection data, and SLR
97 projections to quantify the inundation hazards (probabilities). The proposed approach is applied to analyze the
98 coastal flood hazard for the city of Shanghai, which is within the Northwest Pacific Basin and is highly
99 exposed to typhoon-induced coastal flooding. For instance, Typhoon Winnie (1997) caused storm tides up to
100 nearly 7 meters above Wusong Datum, the highest recorded in Shanghai's history. Meanwhile, Shanghai is
101 protected by high-standard flood defense, which needs to be taken into account when estimating the
102 inundation risk and effects of SLR. The remainder of this paper is organized as follows. Section 2 describes
103 materials and methods, including synthetic TC dataset, storm tide simulation, flood probability analysis, and
104 coastal inundation modeling. Section 3 presents the results and discusses the key findings. Section 4 provides
105 the conclusions and offers suggestions for further research.

106

107 **2. Materials and Methodology**

108

109 **2.1. Historical Events and Flood Protection of Shanghai**

110

111 Shanghai has witnessed frequent extreme flooding induced by TCs. 148 TCs affected the region from 1949 to
112 2015 (Wang et al., 2017), among which 19 and 72 TCs generated storm surges of higher than 1.2 and 0.8 m,
113 respectively. The annual maximum water levels (Fig. S1) were generally caused by the high tides and storm

114 surges. For example, the arrival of Typhoon Winnie's peak surge (2.35 m) coincided with the high
115 astronomical tide, resulting in the highest storm tide (5.99 m) on record in Shanghai. In response to rising
116 record levels, a flood defense system (floodwall along Huangpu River and seawall along the coast) was
117 initiated in 1950s and has been reinforced since then (Fig. S1). Each update of protection standard is triggered
118 by an extreme TC flood event (i.e., typhoons in 1962, 1974, 1981 and 1997), which heavily inundated the city
119 (Xian et al., 2018). At present, Shanghai is protected by 480-km high level (1000-years) floodwalls and 508-
120 km high standard seawalls which are designed to withstand a 100/200-year storm tides plus waves induced by
121 11/12-force winds (Saffir-Simpson Hurricane Category 1). In addition, rainfalls and river discharges are
122 regulated by storm sewer drainage network and the dams/barriers/slucice gates, in order to prevent the
123 compounding effects of pluvial, fluvial and coastal flooding (Yin et al, 2015; Xian et al, 2018).

124

125 **2.2. Synthetic TC Dataset**

126

127 To overcome the limitation of historical data, we estimate TC-induced coastal flood and inundation hazard
128 based on large numbers of synthetic storms. We apply a synthetic TC dataset generated by the deterministic-
129 statistical TC model of Emanuel et al. (2008). This model uses thermodynamic and kinematic statistics of the
130 atmosphere and ocean derived from reanalysis data or climate-model estimation to produce synthetic TCs; it
131 has been widely used to study hurricane wind, storm surge, and rainfall hazards (e.g., Emanuel 2017, Marsooli
132 et al. 2019). Specifically, Xu et al. (2020) applied the synthetic TC model to study typhoon wind hazard for
133 the Shanghai area. We apply the synthetic TC dataset generated in Xu et al. (2020) for the climate over the
134 period of 1979 ~ 2015 based on the National Centers for Environmental Prediction (NCEP) reanalysis
135 (Kalnay et al. 1996). The dataset includes 5018 synthetic storms. Each synthetic storm passes within a 350-

136 km-radius circle centered at a point near Shanghai (latitude 29.86° and longitude 121.56°), and all storms pass
137 within this circle with the maximum wind intensity (1-min wind speed at 10 m above sea level) greater than
138 21 m/s (40 knots). Each storm is characterized by 2-hourly time series of the storm parameters (i.e., time,
139 center position, maximum wind speed, pressure deficit, and radius of maximum wind) required for storm tide
140 modeling. The annual storm frequency associated with the storm set is about 2 storms per year. Xu et al.
141 (2020) found that the estimated wind hazard based on the NCEP synthetic dataset compared well with
142 historical wind observations in the Shanghai region.

143

144 **2.3. Storm Tide Simulation**

145

146 We use the ADvanced CIRCulation model (ADCIRC) to simulate storm tides (i.e., the total water level
147 including storm surge and astronomical tide). ADCIRC, originally developed by Luetlich et al. (1992) and
148 Westerink et al. (1994), is a well-established open-source hydrodynamic model applicable to free surface
149 circulation and transport problems. The model adopts the hydrostatic pressure assumption to numerically
150 solve the governing equations in space and time using, respectively, the finite-element and finite-difference
151 numerical methods. ADCIRC solves the 2-D or 3-D momentum equations to calculate velocity fields. For
152 storm surge modeling in the coastal ocean, the 2-D depth-integrated model is usually preferred to the 3-D
153 model because it is computationally cheaper and largely captures the dominant processes that control the
154 storm-induced water level (Resio and Westerink, 2008). In the present study, we use the 2-D depth-integrated
155 version of ADCIRC. Due to the extremely large computational resource that would be required to simulate
156 wind waves associated with the large number of synthetic storms, we do not apply wave simulations here.
157 Thus we neglect the effect of wave setup on the total water level, which has been estimated to contribute up to

158 10-20% to total extreme water levels in the Shanghai region ([Melet et al., 2018](#)).

159

160 Using the mesh generation module of Surface-water Modeling System (SMS), we develop a computational

161 mesh that extends between latitudes 21°N and 41°N and longitudes 116.5°W and 129.5°W. The computational

162 domain consists of an unstructured triangular mesh with 108,440 nodes and 209,844 elements. The mesh

163 resolution is <100 m nearshore and gradually increases to > 50 km in deeper waters. The bathymetry of the

164 model is based on the bathymetry survey of Yangtze River Estuary in 2012 ([Zhu and Bao, 2016](#)) and GEBCO

165 (GEneral Bathymetric Chart of the Oceans)-2014 global 30 arc sec gridded data

166 (https://www.gebco.net/data_and_products/historical_data_sets/). The vertical datum is in mean sea level

167 (referenced to year 2000). The manning's n bottom roughness coefficient varies spatially over the grid based

168 on a global database for sediments on the seabed (<http://portal.gplates.org/static/html/seafloor.html>). The

169 water level at the open boundaries is specified by eight major tidal constituents (K1, K2, M2, N2, O1, P1, Q1,

170 and S2). The tidal information, including the amplitudes and phases, are obtained from the global model of

171 ocean tides TPXO8-ATLAS with a 1/30° resolution ([Egbert and Erofeeva, 2002](#)). At closed boundaries, i.e.,

172 island and mainland shorelines, the normal flow is set to zero whereas the tangential velocity is determined

173 based on the free-slip boundary condition. While it is difficult to validate the ADCIRC modeling for storm

174 surges in Shanghai, as a critical TC parameter --radius of maximum wind--is not available in the historical

175 record for the Northwest Pacific Basin, the ADCIRC model has been found to produce storm surge

176 estimations with relatively high accuracy in a number of studies (e.g., [Westerink et al., 2008](#); [Marsooli and](#)

177 [Lin, 2018](#)). Our evaluation on the model performance in simulating the astronomical tides, which can

178 contribute to over 75% of the storm tides in Shanghai, shows that the ADCIRC model satisfactorily captures

179 the dominant dynamics of major tide constituents along the Shanghai coast (Fig. S2).

180

181 We use analytical/parametric models to calculate the surface wind and pressure fields associated with the
182 synthetic TCs to drive the hydrodynamic modeling. We use the parametric model of Holland (1980) to
183 calculate the radial profile of pressure, which is related to the maximum wind speed, radius of maximum
184 wind, and pressure deficit. We use the analytical model of Emanuel and Rotunno (2011) to calculate the wind
185 field. The model calculates the 1-min axisymmetric wind field (associated with the storm) at the gradient level
186 based on the storm characteristics including maximum wind speed and radius of maximum wind. We convert
187 the gradient wind to the surface level (10 m above the sea surface) with a velocity reduction factor of 0.85
188 (Georgiou et al., 1983) and an empirical expression of inflow angles (Bretschneider, 1972). We add to the
189 storm wind the surface environmental wind estimated as a fraction (0.55, rotated counter-clockwise by 20°) of
190 the storm translation velocity, to account for the asymmetry of the wind field (Lin and Chavas, 2012). Finally,
191 for use in the ADCIRC modeling we adjust the 1-minute wind to a 10-minute average with a reduction factor
192 of 0.893 (Powell et al., 1996). This framework of TC modeling for storm surge analysis has been implemented
193 by various previous studies (e.g., Lin et al., 2012; Marsooli et al. 2019). Also, Xu et al. (2020) used a similar
194 method to estimate the wind field, and their estimated wind hazard based on the NCEP synthetic dataset
195 compared well with historical wind observations in the Shanghai region.

196

197 **2.4. Flood Probability Analysis**

198

199 Statistical analysis is performed on the generated storm tides for locations/stations at 1000-m intervals along
200 the Shanghai coast. The probability of storm tide events can be estimated by extreme value models such as
201 generalized extreme value distribution family. In this study, the Generalized Pareto Distribution (GPD) is

202 applied to describe the limiting behavior of maximum storm tide values for all individual events using a
203 Peaks-Over-Threshold approach (Simiu and Heckert 1996) and the maximum likelihood method (Lin et al.,
204 2012). The GPD threshold is determined by trial to ensure that the smallest error in the distribution is obtained
205 (Marsooli et al., 2019). Then, the return periods of peak storm time levels are calculated by assuming that the
206 storm arrival for the region is a stationary Poisson process (Lin et al., 2012).

207

208 **2.5. Inland Inundation Modeling**

209

210 A well-established 2D hydraulic model (FloodMap-Inertial, Yu and Lane 2011) is utilized to derive coastal
211 flood inundation for each scenario. The model, as well as its earlier diffusion-based version (FloodMap, Yu
212 and Lane 2006a,b) have been tested and verified in a number of different environments (e.g., Tayefi et al.,
213 2007; Lane et al., 2008; Casas et al., 2010; Yin et al., 2013, 2016, 2019; Yu and Coulthard, 2015). It adopts a
214 simplified 2D solution to numerically solve the inertial form of the 2D shallow water equations by neglecting
215 the convective acceleration term in a raster-based domain. Inland flood routing takes the same structure as the
216 inertial algorithm of Bates et al. (2010), but with a slightly different method to calculate the time step. Rather
217 than using a global Courant–Freidrich–Levy Condition where the time step for the next iteration is calculated
218 based on the maximum water depth and velocity found at the last time step (e.g. Bates and De Roo, 2000), the
219 Forward Courant–Freidrich–Levy Condition (FCFL) approach described in Yu and Lane (2011) for the
220 diffusion-based version of FloodMap is used in the inertial model to maintain simulation stability and
221 minimize numerical diffusion.

222

223 To apply the model for inland flood simulation, two types of data are required: floodplain topography and

224 boundary conditions. In terms of the floodplain topography, a city-wide Digital Elevation Model (DEM)
225 constructed from 0.5 m topographic contours is available (Yin et al., 2013), with a grid cell resolution of 50 m
226 and a vertical accuracy of 0.1-0.2 m. The locations and heights of sea dikes along the coast, provided by
227 Shanghai Water Authority (SWA), are then overlaid onto the original ‘bare earth’ DEM. An empirically-based
228 uniform manning’s n roughness coefficient of 0.06 is used in the simulation to represent the effect of urban
229 features (e.g. buildings) on flood routing. For each synthetic storm, water level time series (every 30 minutes)
230 at locations spaced at 1000 m intervals along the coast, derived from the ADCIRC model run, were used as
231 flow boundary conditions to drive the flood modeling. The performance of the coupled ADCIRC-FloodMap
232 method was investigated by Yin et al., (2016), where the ADCIRC-FloodMap method demonstrated higher
233 efficiency and accuracy in inundation prediction at the city scale than using the ADCIRC model alone, which
234 is particularly important for hazard modeling involving thousands of simulations.

235

236 **3. Results and Discussions**

237

238 **3.1. Probabilistic Flood Hazards**

239

240 For each location along the Shanghai coastline, the return periods of flood levels (storm tides) under the
241 NCAR/NCEP current climate are estimated through the flood probability analysis. The spatially continuous
242 distribution of the estimated flood levels with various return periods (10-, 100- and 1000-year) along the coast
243 is presented in Fig. 1. Results indicate that the flood level substantially increases with the increase of return
244 period: it is between 3.77 and 6.93 m (with an average value of 4.37 m above Wusong Datum) for the 10-year
245 scenario, 4.57 and 8.48 m (5.19 m) for the 100-year scenario, and 5.88 and 12.10m (7.03 m) for the 1000-year
246 scenario. The highest flood return levels (η) and the largest increases in η over the return periods can be

247 observed along the northern coast of Chongming Island. This spatially continuous distribution of simulated
248 flood levels along the coast provides greater detail and accuracy for flood hazard assessment compared to a
249 previous study (Yin et al., 2020), in which flood return levels were interpolated from sparsely distributed tide
250 gauges.

251
252 Fig. 2 displays the flood return level curves at selected gauge stations estimated by our analysis, compared to
253 estimates by SWA using the officially recommended Pearson-III distribution based on annual maximum
254 values of recorded historical water levels. Similar to that shown in Fig. 1, the predicted flood return levels
255 vary greatly from place to place along the coast. For example, the 1000-year flood height is about 7.76 m at
256 Jinshan Station but only about 6.10 m at Luchaogang Station. Only very low-probability events (over 3000 ~
257 10000 year) will exceed the crest levels of seawall. Results also show a large uncertainty in flood levels with
258 long return periods (> 100 years). SWA's analysis predicts significantly higher flood levels, especially for
259 small return periods (e.g., 5 ~ 6 m for the 10-year floods). Peak water levels recorded at the gauge stations
260 during Typhoon Winnie indicate it to be close to a 100-year event by SWA's analysis but an 800 ~ 900-year
261 event by our analysis. This discrepancy can be primarily attributed to the different distribution models and
262 sample data used in the flood probability analyses. The occurrence of Typhoon Winnie may have contributed
263 significantly to lifting the return level curves estimated based on the limited (less than 60 year) historical data.
264 Otherwise, using limited-length historical data often underestimates extremes (Lin et al., 2014; Xu et al.,
265 2020); extrapolating SWA's estimates for return periods greater than 1000 years would result in an
266 underestimation of the extremes compared to our modeling-based estimates.

267

268 **3.2. Worst-case Scenarios**

269

270 The 5180 synthetic storm tide events simulated using ADCIRC are used as boundary conditions to drive
271 inland flood modeling using FloodMap. Given the high level of floodwall protection, there are only a few
272 storms that can cause inundation in Shanghai under the current sea level. Fig. 3a-c shows the spatial pattern of
273 the storm tides and the resultant inundation footprints for three worst-case scenarios in Shanghai in the
274 synthetic simulation under the NCAR/NCEP current climate condition. Typhoon A is a large sized storm that
275 moves northwestward and makes landfall in Jinshan with a high intensity. Due to the wind field's asymmetry,
276 the largest wind forces to the right of the track push surge into Yangtze River Estuary and produce the highest
277 storm tide (over 9 m above Wusong Datum) at the northernmost end of Shanghai. Another relatively strong
278 northwestward-moving storm (Typhoon B) makes landfall in Chongming and induces a comparable storm tide
279 along the northern coast of the island. A smaller-size storm (Typhoon C) which makes landfall farther from the
280 city also generates an extreme sea level during high tide in Hangzhou Bay (8.7 m above Wusong Datum) due
281 to its higher intensity. The three worst-case scenarios have very low probabilities of occurrence (> 5000 years,
282 based on their storm tide return period at the location of the maximum storm tide for each storm, shown by the
283 black star in Fig. 3a-c) and are much higher than the largest storm tides in recorded history (6 ~ 7 m above
284 Wusong Datum).

285

286 The synthetic events cause varying degrees of coastal flood inundation in Shanghai. The highest storm tides
287 due to Typhoon A overwhelm low-lying and poorly-protected coastal floodplains and islands in the Yangtze
288 River Estuary (Fig. 3a). When subject to Typhoon B induced coastal flooding, the inundation area covers
289 about 564 km² in the northeastern part of Chongming Island (Fig. 3b). Particularly, the waterfront areas of
290 western (Typhoon A) and eastern (Typhoon B) Chongming are flooded with maximum water depths higher

291 than 3 m. In contrast, only marginal inundations with shallow water depth (mostly lower than 0.5 m) are
292 observed in the coastal region along Hangzhou Bay under the Typhoon C scenario (Fig. 3c). This relatively
293 small inundation depth can be explained by the presence of lateral topographic confinement and the relatively
294 high crest heights of the seawalls (7 ~ 8 m above Wusong Datum). Pudong New Area and Changxing Island
295 appear to be immune to these extreme flood scenarios, because of their high standard seawalls (8 ~ 11 m
296 above Wusong Datum) and comparatively low storm tides in the lower Yangtze River Estuary. Mainland
297 Shanghai seems to be generally safe from the storm-induced flooding except a small portion of dike-protected
298 hinterland in Baoshan (Fig. 3a). The results presented here highlight the vulnerability of the areas in the upper
299 Yangtze River Estuary where larger storm tides develop and which have relatively low levels of seawall
300 protection, such as Chongming Island and Baoshan.

301

302 **3.3. SLR impact on flooding**

303

304 Yin et al. (2020) provided the probabilistic SLR projections for Shanghai, which take into account both
305 climatic and non-climatic (subsidence) components, under three Representative Concentration Pathways
306 (RCP 2.6, 4.5 and 8.5) by the end of 21st century, relative to the baseline year of 2010. The median (50th
307 percentile) estimates under RCP 8.5 are used here to investigate the effect of local relative SLR on typhoon-
308 induced coastal flooding and inundation. We find that the projected SLR would lead to non-linear impact on
309 flood and inundation hazards. For example, the 3000-year flood level at the Jinshan station (at the height of
310 the seawall to cause inundation) would become a less than 1000- and 900-year flood events in the mid- and
311 end-of-twenty-first century, respectively (Fig. 2). Overall in Shanghai, compared with the current situation,
312 typhoon-induced flood inundation would occur two times more frequently with a 0.5-m SLR by 2050 and 20

313 times more frequently with a 1.36-m SLR by 2100.

314

315 Inundation severity will also significantly increase. Fig. 3d-i display the derived coastal flood inundations for
316 the three worst-cases under the 2050 and 2100 sea levels. A cross comparison between Fig. 3a-c and Fig. 3d-i
317 reveals that extreme typhoon-induced coastal inundations in Shanghai, as expected, would increase
318 significantly under SLR. Although the general patterns of inundation are characterized by a certain degree of
319 consistency between the current and 2050 scenarios, the flooded areas are projected to increase by 26%, 24%,
320 and 437% for Typhoon A, B and C, respectively. Meanwhile, the projected SLR of 0.5 m could contribute to a
321 23%, 19% and 74% rises in the average inundation depth for the three cases, respectively. If the local sea level
322 is raised by 1.36 m by the end of the century, the predicted inundation areas for Typhoon A, B, and C will be
323 respectively 60%, 110% and 1360% larger than those with the present-day sea level, and the average
324 inundation depth will increase respectively by 69%, 16% and 141%. Extreme flood hazards caused by
325 Typhoon A and B would almost totally inundate the Chongming and Hengsha islands by 2100. Without an
326 upgraded flood defense, Baoshan and the coastal districts along Hangzhou Bay could also be greatly affected
327 by Typhoon A and C under the 2100 SLR.

328

329 **4. Conclusions**

330

331 In this work, we develop a combined hurricane-circulation-inundation model to quantify extreme coastal
332 flooding induced by synthetic storms under current and future sea levels in Shanghai, China. The main
333 conclusions are summarized as follows: 1) although the storm tide hazard is high, Shanghai's flood protection
334 system is sufficient for preventing majority of the city from severe flooding (> 100 years) from storm tide

335 under the current climate; 2) extreme “worst-case” scenarios (> 5000 years) can generate unprecedented storm
336 tides (8 - 9 m) in Yangtze River Estuary or Hangzhou Bay, even under the current climate; 3) future SLR will
337 greatly increase Shanghai’s flooding risk compared to the current state, with inundation two times and 20
338 times more likely to occur by mid- and late-21st century, respectively, and inundation depth and area to greatly
339 increases (e.g., 60-1360% increase in the inundation area for the “worst cases” by 2100).

340

341 The present study contributes to a better understanding of extreme coastal flooding from TC-induced storm
342 tide and SLR in Shanghai and unlocks the potential for estimating flood hazard evolution due to SLR as well
343 as storm change (e.g., [Marsooli et al., 2019](#)) in a changing climate. The methodology is applicable to any
344 coastal city that is susceptible to TC surge flooding and rising sea level. However, since we neglect wave
345 effects on the water level, major seawall failure mechanisms such as wave overtopping and breaching are not
346 considered in the present storm flood modeling; the inundation risk estimated herein is likely a lower bound.
347 Further work will include wave modeling and dike reliability analysis (e.g., [Yin et al., 2020](#)) in the
348 climatological-hydrodynamic modeling to better quantify the flood risk under both the current and future
349 climate conditions.

350

351 **Acknowledgments**

352 This paper was supported by the National Key Research and Development Program of China (Grant no:
353 2018YFC1508803, 2017YFE0107400, 2017YFE0100700), the National Natural Science Foundation of China
354 (Grant no: 41871164, 51761135024), the Fundamental Research Funds for the Central Universities (Grant no:
355 2018ECNU-QKT001, 2017ECNUKXK013), the Institute of Eco-Chongming (Grant no: ECNU-IEC-202001),
356 and the National Science Foundation of the United States (grant EAR-1520683). We also thank Professor
357 Kerry Emanuel (MIT) for generating the synthetic TC dataset and Professor Jianrong Zhu (ECNU) for
358 providing us with the high-resolution bathymetry data. Data is available through Xu et al. 2020 and Yin et al.
359 2020. Model simulations presented in this study are available for download through DOI
360 10.6084/m9.figshare.12911630.

361

362

363 **References**

- 364 Aerts J C, Lin N, Botzen W J, Emanuel K, Moel H, 2013. Low-probability flood risk modeling for New York
365 City, *Risk Analysis*, 33: 772-788.
- 366 Barnard, P.L., Erikson, L.H., Foxgrover, A.C., Hart, J.A.F., Limber, P., O'Neill, A.C., van Ormondt, M.,
367 Vitousek, S., Wood, N., Hayden, M.K., Jones, J.M., 2019. Dynamic flood modeling essential to assess
368 the coastal impacts of climate change. *Scientific Reports*, 9: 4309.
- 369 Bates P D, De Roo A P J, 2000. A simple raster-based model for flood inundation simulation. *Journal of*
370 *Hydrology*, 236: 54-77.
- 371 Bates P D, Horritt M, Fewtrell T, 2010. A simple inertial formulation of the shallow water equations for
372 efficient two-dimensional flood inundation modelling. *Journal of Hydrology*, 387(1-2): 33-45.
- 373 Batts M E, Cordes M R, Simiu E, 1980. Sampling errors in estimation of extreme hurricane winds. *Journal of*
374 *the Structural Division-ASCE*, 106: 2109-2115.
- 375 Blake E S, Kimberlain T B, Berg R J, Cangialosi J P, Beven J L, 2013. Tropical cyclone report hurricane
376 sandy (Rep. AL182012). Miami, FL: National Hurricane Center.
- 377 Bretschneider C, 1972. A non-dimensional stationary hurricane wave model. Paper presented at Offshore
378 Technology Conference, Houston, TX (Pap. OTC 1517).
- 379 Casas A, Lane, S N, Yu D, Benito G, 2010. A method for parameterising roughness and topographic sub-grid
380 effects in hydraulic modeling from LiDAR data. *Hydrology and Earth System Sciences*, 14 (8): 1567-
381 1579.
- 382 Egbert G D, Erofeeva S Y, 2002. Efficient inverse modeling of barotropic ocean tides. *Journal of Atmospheric*
383 *and Oceanic Technology*, 19: 183-204.
- 384 Emanuel K, Sundararajan R, Williams J, 2008. Hurricanes and global warming: Results from downscaling
385 IPCC AR4 simulations. *Bulletin of the American Meteorological Society*, 89: 347-368.
- 386 Emanuel K A, Rotunno R, 2011. Self-stratification of tropical cyclone outflow. Part I: Implications for storm
387 structure. *Journal of Atmospheric Sciences*, 68: 2236-2249.
- 388 Emanuel K A, 2013. Downscaling CMIP5 climate models shows increased tropical cyclone activity over the
389 21st century. *Proceedings of the National Academy of Sciences of United States of America*, 110(30):
390 12219-12224.
- 391 Georgiou P N, Davenport A G, Vickery P J, 1983. Design wind speeds in regions dominated by tropical
392 cyclones. *Journal of Wind Engineering and Industrial Aerodynamics*, 13: 139-152.
- 393 Hallegatte S, Green C, Nicholls R J, Corfee-Morlot J, 2006. Future flood losses in major coastal cities. *Nature*
394 *Climate Change*, 3: 802-806.
- 395 Holland G J, 1980. An analytical model of the wind and pressure profiles in hurricanes. *Monthly Weather*
396 *Review*, 108(8): 1212-1218.
- 397 Jelesnianski C P, Chen J, Shaffer W A, 1992. SLOSH: Sea, lake, and overland surges from hurricanes.
- 398 Jing R, Lin N, 2020. An environment-dependent probabilistic tropical cyclone model. *Journal of Advances in*
399 *Modeling Earth Systems*, 12: e2019MS001975.
- 400 Kalnay E, Kanamitsu M, Kistler R, Collins W, Deaven D, Gandin L, Iredell M, Saha S, White G, Woollen J,
401 Zhu Y, Leetmaa A, Reynolds R, Chelliah M, Ebisuzaki W, Higgins W, Janowiak J, Ropelewski K,
402 Wang J, Jenne R, Dennis J, 1996. The NCEP/NCAR 40-year reanalysis project. *Bulletin of American*
403 *Meteorological Society*, 77 (3): 437-471.
- 404 Kates R W, Colten C E, Laska S, Leatherman S P, 2006. Reconstruction of New Orleans after Hurricane

405 Katrina: A research perspective. *Proceedings of the National Academy of Sciences of United States of*
406 *America*, 103: 14653-14660.

407 Knutson T, Camargo S J, Chan J C L, Emanuel K, Ho C-H, Kossin J, Mohapatra M, Satoh M, Sugi M, Walsh
408 K, Wu L, 2020. Tropical Cyclones and Climate Change Assessment: Part II: Projected Response to
409 Anthropogenic Warming. *Bulletin of the American Meteorological Society*, 101(3): E303–E322.

410 Lane S N, Reid S C, Tayefi V, Yu D, Hardy R J. Reconceptualising coarse sediment delivery problems in
411 rivers as catchment-scale and diffuse. *Geomorphology*, 2008, 98(34): 227-249.

412 Lin N, Emanuel K A, Smith J A, Vanmarcke E, 2010. Risk Assessment of Hurricane Storm Surge for New York City. *Journal*
413 *of Geophysical Research*, 115: D18121.

414 Lee C Y, Tippett M K, Sobel A H, Camargo S J, 2018. An environmentally forced tropical cyclone hazard
415 model. *Journal of Advances in Modeling Earth Systems*, 10, 223-241.

416 Lin N, Emanuel K A, Smith J A, Vanmarcke E, 2010. Risk Assessment of Hurricane Storm Surge for New
417 York City. *Journal of Geophysical Research*, 115 (D18): D18121.

418 Lin N, Chavas D, 2012. On hurricane parametric wind and applications in storm surge modeling. *Journal of*
419 *Geophysical Research*, 117: D09120.

420 Lin N, Lane P, Emanuel K A, Sullivan R M, Donnelly J P, 2014. Heightened hurricane surge risk in northwest
421 Florida revealed from climatological-hydrodynamic modeling and paleorecord reconstruction. *Journal of*
422 *Geophysical Research*, 119(14): 8606-8623.

423 Lin N, Emanuel K, Oppenheimer M, Vanmarcke E, 2012. Physically based assessment of hurricane surge
424 threat under climate change. *Nature Climate Change*, 2: 462-467.

425 Lin N, Shullman E, 2017. Dealing with Hurricane Surge Flooding in a Changing Environment: Part I. Risk
426 Assessment Considering Storm Climatology Change, Sea Level Rise, and Coastal Development.
427 *Stochastic Environmental Research and Risk Assessment*, 31: 2379-2400.

428 Lin N, Kopp R E, Horton B P, Donnelly J P, 2016. Hurricane Sandy’s Flood Frequency Increasing from Year
429 1800 to 2100. *Proceedings of the National Academy of Sciences of the United States*, 113 (43): 12071-
430 12075.

431 Luettich R A, Westerink J J, Scheffner N W, 1992. ADCIRC: An advanced three-dimensional circulation
432 model for shelves, coasts and estuaries. Report 1. Theory and methodology of ADCIRC-2DDI and
433 ADCIRC-3DL (Tech. Rep. DRP-92-6). Vicksburg, MS: U.S. Army Corps of Engineers.

434 Marsooli R, Lin N, 2018. Numerical modeling of historical storm tides and waves and their interactions along
435 the U.S. east and Gulf Coasts. *Journal of Geophysical Research: Oceans*, 123: 3844-3874.

436 Marsooli R, Lin N, Emanuel K, Feng K. Climate change exacerbates hurricane flood hazards along US
437 Atlantic and Gulf Coasts in spatially varying patterns. *Nature Communications*, 2019, 10: 3785.

438 Melet, A., Meyssignac, B., Almar, R., Le Cozannet, G., 2018. Under-estimated wave contribution to coastal
439 sea-level rise. *Nature Climate Change*, 8(3), 234–239. doi:10.1038/s41558-018-0088-y

440 Powell M D, Houston S H, Reinhold T A, 1996. Hurricane Andrew’s landfall in South Florida. Part I:
441 standardizing measurements for documentation of surface wind fields. *Weather Forecast.* 11: 304-328.

442 Resio, D.T., Westerink, J.J., 2008. Modeling the physics of storm surges. *Physics Today*, 61(9), 33–38.
443 doi:10.1063/1.2982120

444 Simiu E, Heckert N A. Extreme wind distribution tails: a peak over threshold approach. *Journal of Structural*
445 *Engineering (ASCE)*, 1996, 122: 539-547.

446 Smith A B, Katz R W. US billion-dollar weather and climate disasters: Data sources, trends, accuracy and
447 biases. *Natural Hazards*, 2013, 67: 387-410.

448 Tayefi V, Lane S N, Hardy R J, Yu D. A comparison of one- and two-dimensional approaches to modelling
449 flood inundation over complex upland floodplains. *Hydrological Processes*, 2007, 21(23): 3190-3202.

450 Vitousek, S., Barnard, P.L., Fletcher, C.H., Frazer, N., Erikson, L., Storlazzi, C.D., 2017. Doubling of coastal
451 flooding frequency within decades due to sea-level rise. *Scientific Reports*, 7: 1399. doi:10.1038/s41598-
452 017-01362-7

453 Vickery P J, Skerjil P F, Twisdale L A, 2000. Simulation of hurricane risk in the U.S. using empirical track
454 model. *Journal of Structural Engineering*, 126: 1222-1237.

455 Vickery P J, Wadhwa D, Twisdale L A Jr, Lavelle F M, 2009. U.S. hurricane wind speed risk and uncertainty.
456 *Journal of Structural Engineering*, 135: 301-320.

457 Wang J, Huang H, Zhang C, Liu J, Yan J, Geng L, 2017. The preventive measures to deal with the disaster of
458 storm surge of Shanghai city. *Ocean Development and Management*, 2017, 34(1):92-96. (In Chinese)

459 Westerink J J, Luettich R A, Blain C A, Scheffner N W, 1994. ADCIRC: An advanced three-dimensional
460 circulation model for shelves, coasts and estuaries. Report 2: Users' manual for ADCIRC-2DDI (Tech.
461 Rep. DRP-92-6). Vicksburg, MS: U.S. Army Corps of Engineers.

462 Westerink J J, Luettich R A, Feyen J C, Atkinson J H, Dawson C, Roberts H J, Powell M D, Dunion J P,
463 Kubatko E J, Pourtaheri H, 2008. A basin- to channel-scale unstructured grid hurricane storm surge
464 model applied to Southern Louisiana. *Monthly Weather Review*, 136(3), 833-864.

465 Woodruff J D, Irish J L, Camargo S J, 2013. Coastal flooding by tropical cyclones and sea-level rise. *Nature*,
466 504: 44-52.

467 Xian S, Yin J, Lin N, Oppenheimer M, 2018. Influence of Risk Factors and Past Events on Flood Resilience
468 in Coastal Megacities: Comparative Analysis of NYC and Shanghai. *Science of the Total Environment*,
469 2018, 610-611C: 1251-1261.

470 Xu H, Lin N, Huang M, Lou W, 2020. Design tropical cyclone wind speed when considering climate change.
471 *ASCE Journal of Structural Engineering*, 146(5): 04020063.

472 Yin J, Yu D P, Yin Z E, Wang J, Xu S Y, 2013. Modelling the combined impacts of sea-level rise and land
473 subsidence on storm tides induced flooding of the Huangpu River in Shanghai, China. *Climatic Change*,
474 2013, 119(3): 919-932.

475 Yin J, Yu D P, Yin Z E, Wang J, Xu S Y, 2015. Modelling the anthropogenic impacts on fluvial flood risks in
476 a coastal mega-city: A scenario-based case study in Shanghai, China. *Landscape and Urban Planning*,
477 136: 144-155.

478 Yin J, Lin N, Yu D. Coupled modeling of storm surge and coastal inundation: a case study in New York City
479 during Hurricane Sandy. *Water Resources Research*, 2016, 52: 8685-8699.

480 Yin J, Zhao Q, Yu D, Lin N, Kubanek J, Ma G, Liu M, Pepe A. Long-term flood-hazard modeling for coastal
481 areas using InSAR measurements and a hydrodynamic model: the case study of Lingang New City,
482 Shanghai. *Journal of Hydrology*, 2019, 571: 593-604.

483 Yin J, Jonkman S, Lin N, Yu D, Aerts J, Wilby R, Pan M, Wood E, Bricker J, Ke Q, Zeng Z, Zhao Q, Ge J,
484 Wang J. Flood risks in sinking delta cities: time for a re-evaluation? *Earth's Future*, 2020, 8:
485 e2020EF001614.

486 Yu D, Lane S N, 2006a. Urban fluvial flood modelling using a two-dimensional diffusion wave treatment,
487 part 1: mesh resolution effects. *Hydrological Processes*, 20: 1541-1565.

488 Yu D, Lane S N, 2006b. Urban fluvial flood modelling using a two-dimensional diffusion wave treatment,
489 part 2: development of a sub grid-scale treatment. *Hydrological Processes*, 20: 1567-1583.

490 Yu D, Lane S N, 2011. Interaction between subgrid-scale resolution, feature representation and grid-scale

491 resolution in flood inundation modelling. *Hydrological Processes*, 25: 36-53.
492 Yu D, Coulthard T J, 2015. Evaluating the importance of catchment hydrological parameters for urban surface
493 water flood modelling using a simple hydro-inundation model. *Journal of Hydrology*, 524: 385-400.
494 Zhu J, Bao D, 2016. The effects of river regime changes in the Changjiang Estuary on hydrodynamics and
495 salinity intrusion in the past 60 years I. River regime changes. *Haiyang Xuebao*, 2016, 38(12): 11-22. (In
496 Chinese)

497
498

499 **Figure Captions**

500

501 Fig. 1 Estimated storm tide levels (m above Wusong Datum) along the Shanghai region coast for 10- (a), 100-
502 (b) and 1000-year (c) return periods under the current climate.

503

504 Fig. 2 Estimated flood return period curves at six selected gauge stations around Shanghai for the
505 NCAR/NCEP current climate (black) and 2050 (0.5 m; orange) and 2100 (1.36 m; purple) sea levels. The x
506 axis is the return period (year) and the y axis is the flood level (m above Wusong Datum). The shade area
507 represents the 95% confidence interval. The green line represents the crest level of seawall at the gauge
508 stations. The red line represents the peak water level recorded at gauge stations during Typhoon Winnie. The
509 blue dot represents the flood return period level estimated by SWA using a Pearson-III distribution based on
510 annual maximum values of recorded historical water levels at the gauge stations.

511

512 Fig. 3 Three worst-case coastal flood inundation scenarios in Shanghai. (a-c) Typhoon A, B and C induced
513 coastal inundations under the current climate; (d-f) Typhoon A, B and C induced coastal inundations under the
514 2050 sea level (0.5 m); (g-i) Typhoon A, B and C induced flood inundations under the 2100 sea level (1.36 m).
515 The black curve in the insert shows the storm track and the black star shows the location with the maximum
516 water level during the storm (a, b, c). The storm parameters at landfall are: (a, d, g) Typhoon A: maximum
517 wind speed $V_m = 46.9$ m/s, minimum sea-level pressure $P_c = 958.8$ mb, radius of maximum wind $R_m = 81.2$
518 km, and translation speed $U_t = 13.4$ m/s; (b, e, h) Typhoon B: $V_m = 51.0$ m/s, $P_c = 952.4$ mb, $R_m = 80.1$ km, and
519 $U_t = 9.0$ m/s; (c, f, j) Typhoon C: $V_m = 52.0$ m/s, $P_c = 951.5$ mb, $R_m = 63.7$ km, and $U_t = 6.7$ m/s.

520

521

522

523

524

525

526

527

528

529

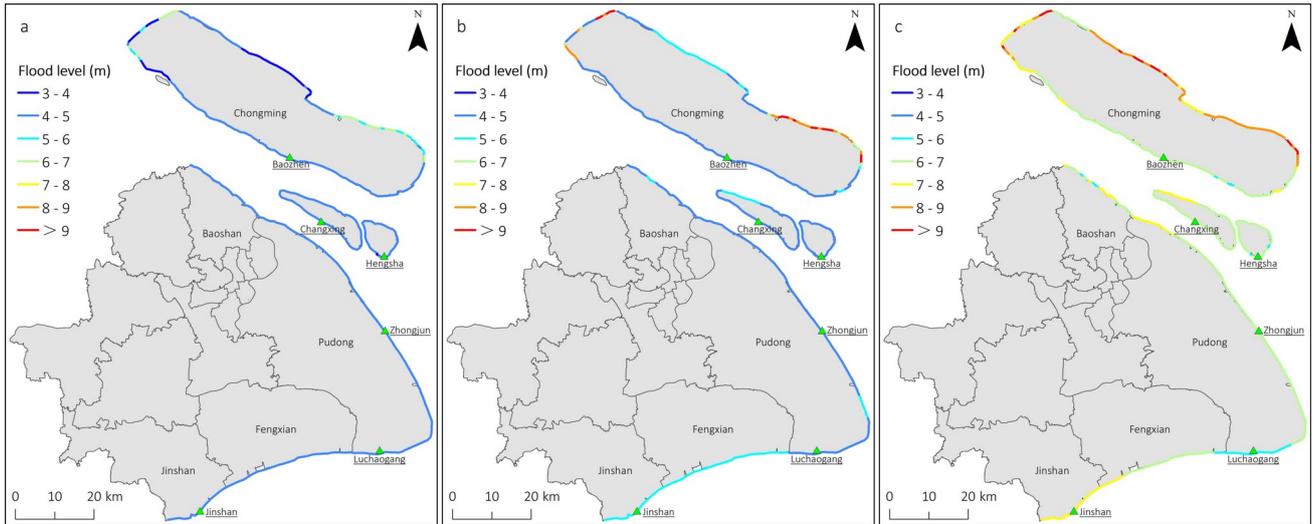
530

531

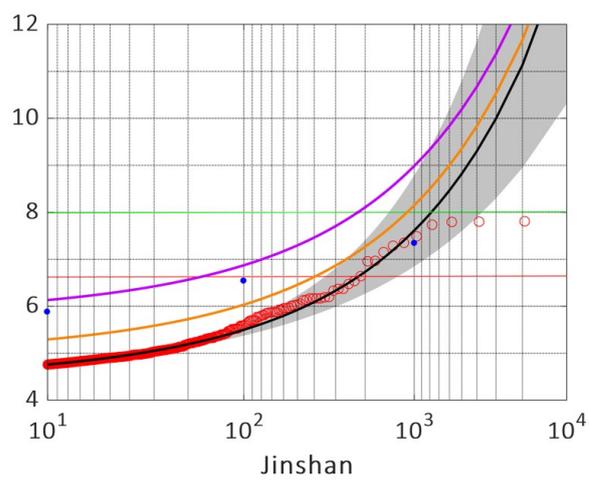
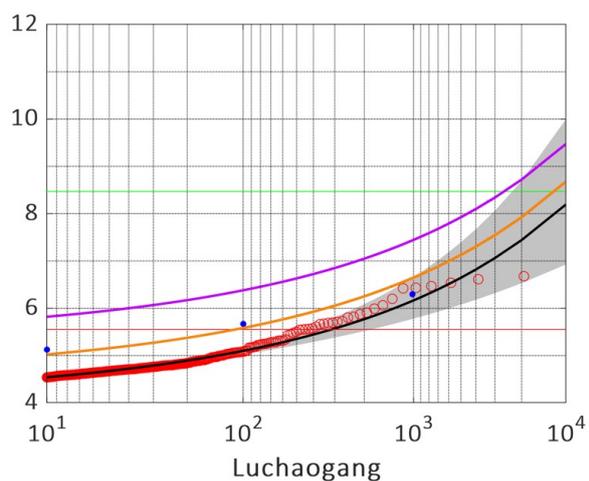
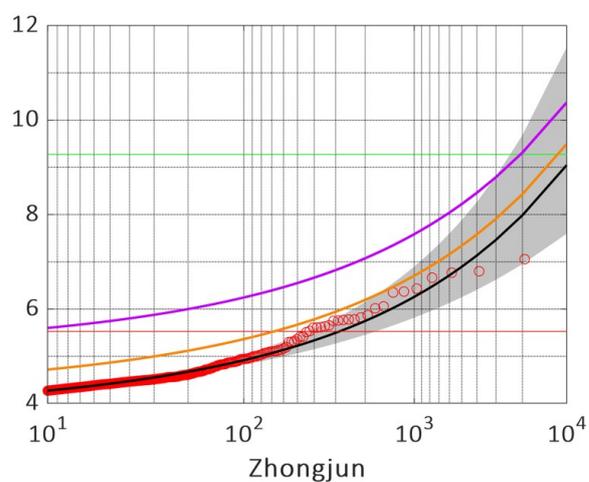
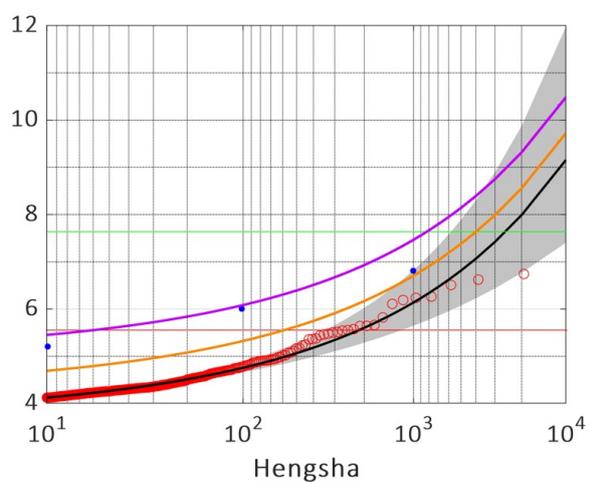
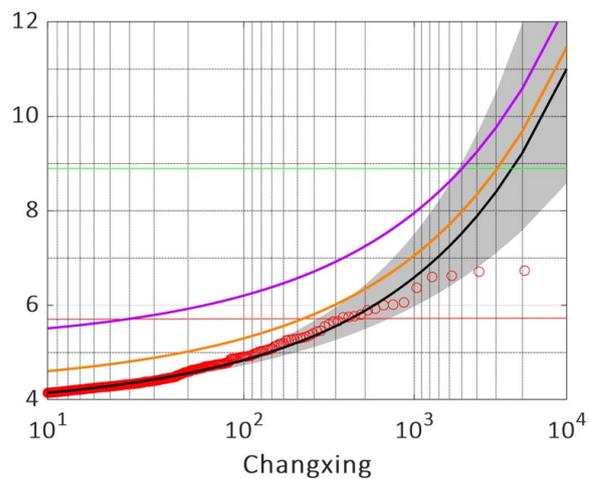
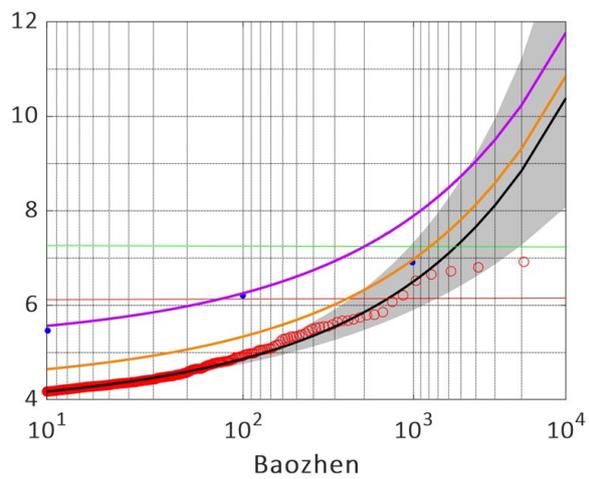
532

533

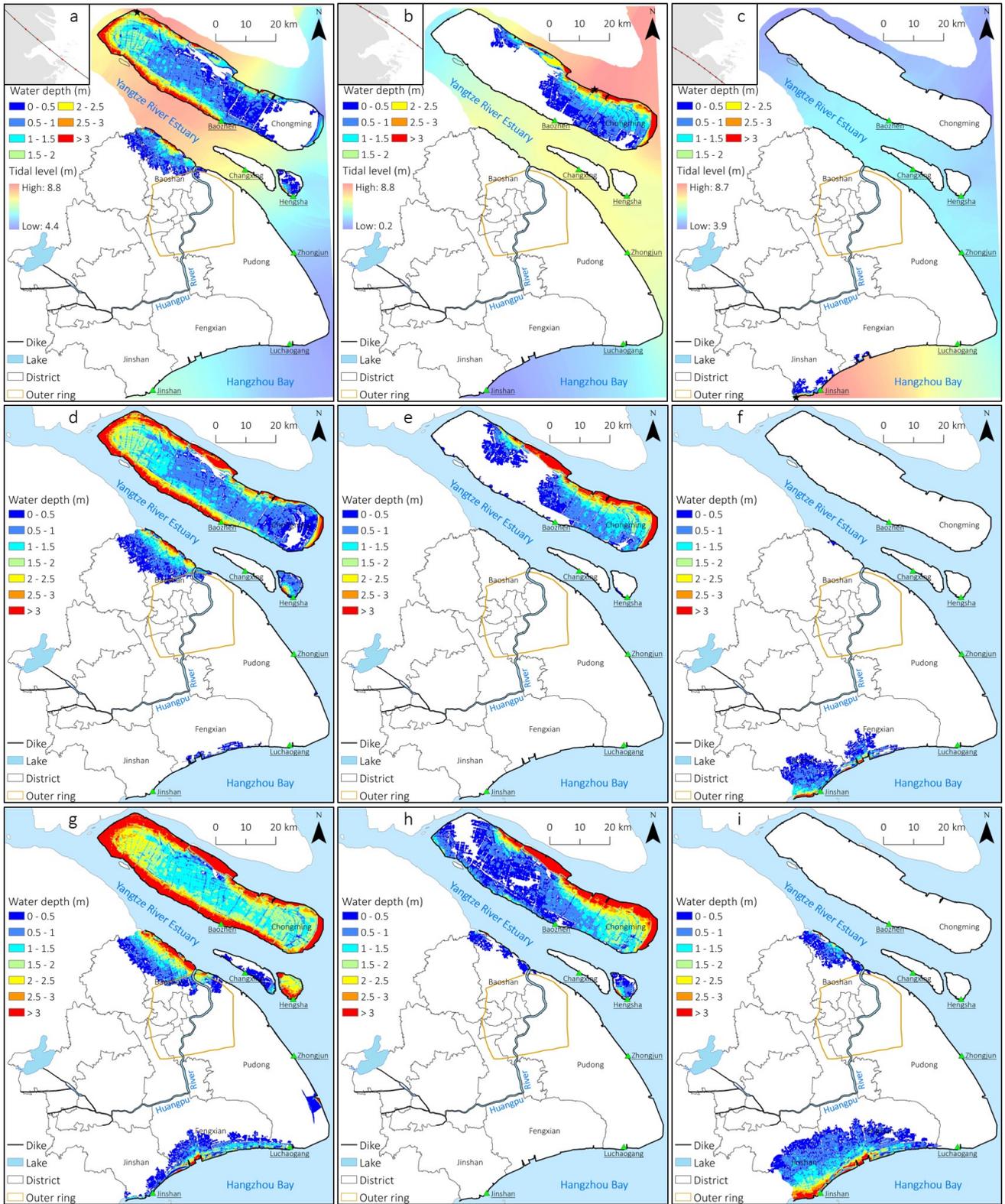
534
535
536
537
538
539
540
541
542



543
544



545



546