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Supporting Information for

**Melting Experiments on Fe-O-H and Fe-H: Evidence for Eutectic Melting in Fe-FeH
and Implications for Hydrogen in the Core**

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Experimental Methods

Melting experiments on the Fe-O-H system. We used diamond anvils with flat 300 μm or single-beveled 120 μm culet size for experiments on Fe-O \pm H (Table S1). A pure Fe (5N, *Mairon-UHP*, *Toho Zinc*) or Fe-12wt%O foil, same as that used in Oka et al. (2019), was loaded into a hole at the center of a pre-indented rhenium gasket, together with a powder mixture of Al(OH)₃ and Al₂O₃ (a source of oxygen and hydrogen) and 10 μm -thick Al₂O₃ sapphire single crystals (thermal insulation layers). Upon heating, Al(OH)₃ dehydrates to form AlOOH or Al₂O₃. The mixing ratio between Al₂O₃ and Al(OH)₃ was varied in order to change the Fe/H₂O ratio of a system.

The sample was heated from both sides with a couple of 100W single-mode Yb fiber lasers with flat-top beam-shaping optics. The laser spot size was 20–30 μm across. The heating duration was limited to less than 3 sec to avoid temperature fluctuations which could lead to a complex melting texture. Indeed, it is long enough for O and H to diffuse over a melt pocket (Helffrich, 2014), which assures chemical equilibrium between liquid and solid when considering that melting/crystallization at the liquid-solid boundary occurs almost instantaneously (Yokoo et al., 2019; Hasegawa et al., 2021). According to previous time-series melting experiments on the Fe-S system, the compositions of coexisting liquid and solid did not change after heating for 1 sec in a laser-heated DAC (Mori et al., 2017). The diffusivities of O and H in molten iron are higher than that of S (Helffrich, 2014). A temperature profile was obtained using a spectro-radiometric method (Hirao et al., 2020). The temperature at the liquid/solid boundary corresponds to the liquidus temperature of a liquid obtained in each run. We determined it by combining the temperature profile with a sample cross-section (e.g., Mori et al., 2017; Tateno et al., 2018; Oka et al., 2019) (Figure 2c).

We performed XRD measurements in-situ at high P - T using an X-ray beam with energy of ~ 30 keV at the beamline BL10XU, SPring-8 (Figure 1). XRD spectra were collected on a flat panel detector (FPD, *Perkin Elmer*) with exposure time of 1 sec before and after heating at 300 K and of 0.2 sec continuously during laser heating. The IPAnalyzer software (Seto et al., 2010) was used to integrate two-dimensional XRD image into one-dimensional diffraction profile. Sample pressure was measured at 300 K after heating based on the unit-cell volume of Al₂O₃ corundum and its equation of state (Dewaele & Torrent, 2013). We considered that 60% and 90% of theoretical thermal pressure for purely isochoric heating, $\Delta P = \alpha K_T \times (T - 300)$ ($\alpha K_T = 4$ and 9 MPa/K), contributed to an increase in sample pressure during heating at ~ 40 GPa and ~ 150 GPa, respectively (e.g., Hirose et al., 2019; Oka et al., 2019).

Textural and chemical characterizations except for H (see below) were carried out on each recovered sample; it is well known that H escapes from metal Fe when it transforms into bcc during decompression (e.g., Iizuka-Oku et al., 2017; Tagawa et al., 2021). A sample cross-section and X-ray elemental maps were obtained parallel to the compression axis by a focused ion beam (FIB, *FEI Versa 3D DualBeam*) and an energy-dispersive spectroscopy (EDS) attached to a field-emission (FE)-type scanning electron microscope (SEM) (Figures 2a, b). Quantitative chemical analyses were then made for coexisting liquid and crystals (liquidus phases) with an FE-type electron probe micro-analyzer (FE-EPMA, *JEOL JXA-8530F*) with an accelerating voltage of 12 kV, a current of 15 nA, and the X-ray counting time of 20/10 sec for peak/background. Fe, Fe₃C, and corundum were used as standards. LIF (Fe), LDE2H (C), TAP (Al), and LDE1 (O) were analyzing crystals. The FE-EPMA analyses of quenched liquid Fe sometimes included a small amount of Al, which is likely a signal from the surrounding pressure medium or Al₂O₃ grains that mechanically intruded into the liquid; note that the amount of Al incorporated into liquid Fe metal is negligible (Badro et al., 2016; Helffrich et al., 2020). Al was therefore subtracted as Al₂O₃ from raw data. C was detected not only in the quenched liquid but also inside the rhenium gasket; the latter could be due to contamination during FIB and/or FE-EPMA analysis. Thus, we subtracted 0.2–0.4 wt% C from the raw analyses of liquids, which was found on the rhenium gasket in the same sample cross-section. The liquid should have included the remaining 0.1–3.7 wt% C (Table S1).

H concentration, x in FeH _{x} , was estimated from its lattice volume (Hirose et al., 2019; Tagawa et al., 2021), which expands proportionally to the H content (Caracas, 2015);

$$x = \frac{V_{\text{FeH}_x} - V_{\text{Fe}}}{\Delta V_{\text{H}}}, \quad (1)$$

where V_{FeH_x} and V_{Fe} are the unit-cell volumes of FeH _{x} and Fe (Dorogokupets et al., 2017 for fcc Fe and Dewaele et al., 2006 for hcp Fe), respectively, and ΔV_{H} is an increase in the lattice volume of Fe per H atom from Caracas (2015). Note that theoretically-derived ΔV_{H} for the hcp phase at 0 K by Caracas (2015) is quite consistent with the room-temperature ΔV_{H} obtained experimentally for fcc by Tagawa, Gomi et al. (2022). The error in the H content, x , is estimated to be $\pm 8\%$ at maximum, which is mainly derived from uncertainty in ΔV_{H} (Ikuta et al., 2019; Tagawa et al., 2021).

Melting experiment on the Fe-H system. We have also conducted a melting experiment on the Fe-FeH binary system (Table S2), using a laser-heated DAC with beveled 200 μm culet anvil. A 10- μm thick pure iron foil was loaded between the pellets

of Al_2O_3 powder. A whole DAC was dried in a vacuum oven at 393 K for at least 1 hr and subsequently at 350 K for 30 min in a vacuumed hydrogen-loading system.

Hydrogen was cryogenically loaded into a sample chamber (Chi et al., 2011). After the chamber was filled with liquid hydrogen, sample was compressed at ~ 15 K and then restored to room temperature. The surface of the diamond anvils was coated with a thin layer of Ti by sputtering (Ohta et al., 2015) in order to avoid anvil failure. We synthesized the FeH_x sample at 10 GPa and melted it at 45 GPa with in-situ XRD measurements at BL10XU, SPring-8 (Figure 1b). We obtained pressures from the Raman shift of a diamond anvil (Akahama & Kawamura, 2004) and from the lattice volume of Al_2O_3 corundum when XRD data were available (Dewaele & Torrent, 2013). The temperature at the liquid/solid boundary was found to be 1900 K in the temperature profile considering the width of a liquid pool estimated by scanning the sample with respect to an X-ray beam. Other procedures including the determination of the H contents in solid and liquid Fe phases were similar to those for the $\text{Fe-O}\pm\text{H}$ sample described above.

Table S1*Experimental Results on the Fe-O±H System*

| Run # | Starting materials | P (GPa) at high T | P (GPa) at 300 K | T (K) | Liquid composition | | | Liquidus phase |
|-------|---|--------------------------|-----------------------|-----------|--------------------|---------|----------|-----------------------|
| | | | | | O (wt%) | H (wt%) | C (wt%) | |
| A1 | Fe-12wt%O + Al ₂ O ₃ + Al(OH) ₃ ^a | 35(2) | 30(2) | 2460(120) | 3.53(4) | 0.27(2) | 1.68(9) | FeO |
| A2 | Fe-12wt%O + Al ₂ O ₃ + Al(OH) ₃ ^b | 37(2) | 32(2) | 2470(110) | 7.20(4) | 0.18(1) | 0.11(9) | FeO |
| A3 | Fe-12wt%O + Al ₂ O ₃ + Al(OH) ₃ ^b | 41(2) | 36(2) | 2400(120) | 9.53(18) | 0.22(2) | 0.20(12) | FeO |
| A4 | Fe + Al(OH) ₃ | 39(2) | 33(2) | 2370(120) | 2.98(29) | 0.49(4) | 0.43(4) | Fe ^d + FeO |
| A5 | Fe + Al ₂ O ₃ + Al(OH) ₃ ^c | 147(15) | 122(12) | 3200(320) | 12.97(86) | 0.00(0) | 0.86(7) | Fe |
| A6 | Fe + Al ₂ O ₃ + Al(OH) ₃ ^c | 160(16) | 136(14) | 3200(320) | 10.36(56) | 0.04(0) | 3.74(23) | FeO |

^aAl₂O₃ : Al(OH)₃ = 10 : 3 by weight^bAl₂O₃ : Al(OH)₃ = 10 : 4 by weight^cAl₂O₃ : Al(OH)₃ = 10 : 8 by weight^dcontains 0.43(3) wt% H calculated from its unit-cell volume of 20.5 Å³**Table S2***Experimental Results on the Fe-H System*

| Run # | P (GPa) | T (K) | solid hcp-FeHx | | | | quenched liquid hcp-FeHx | | | |
|-------|-----------|-----------|----------------|----------|-----------------------|---------|--------------------------|----------|-----------------------|---------|
| | | | a (Å) | c (Å) | V (Å ³) | x | a (Å) | c (Å) | V (Å ³) | x |
| B | 10(1) | 300 | 2.528(1) | 4.067(3) | 22.51(8) | 0.30(2) | | | | |
| | 45(2) | 1900(100) | 2.426(5) | 3.969(7) | 20.23(24) | | | | | |
| | 41(2) | 300 | 2.422(0) | 3.894(1) | 19.78(3) | 0.20(2) | 2.418(2) | 3.948(5) | 20.00(13) | 0.26(2) |

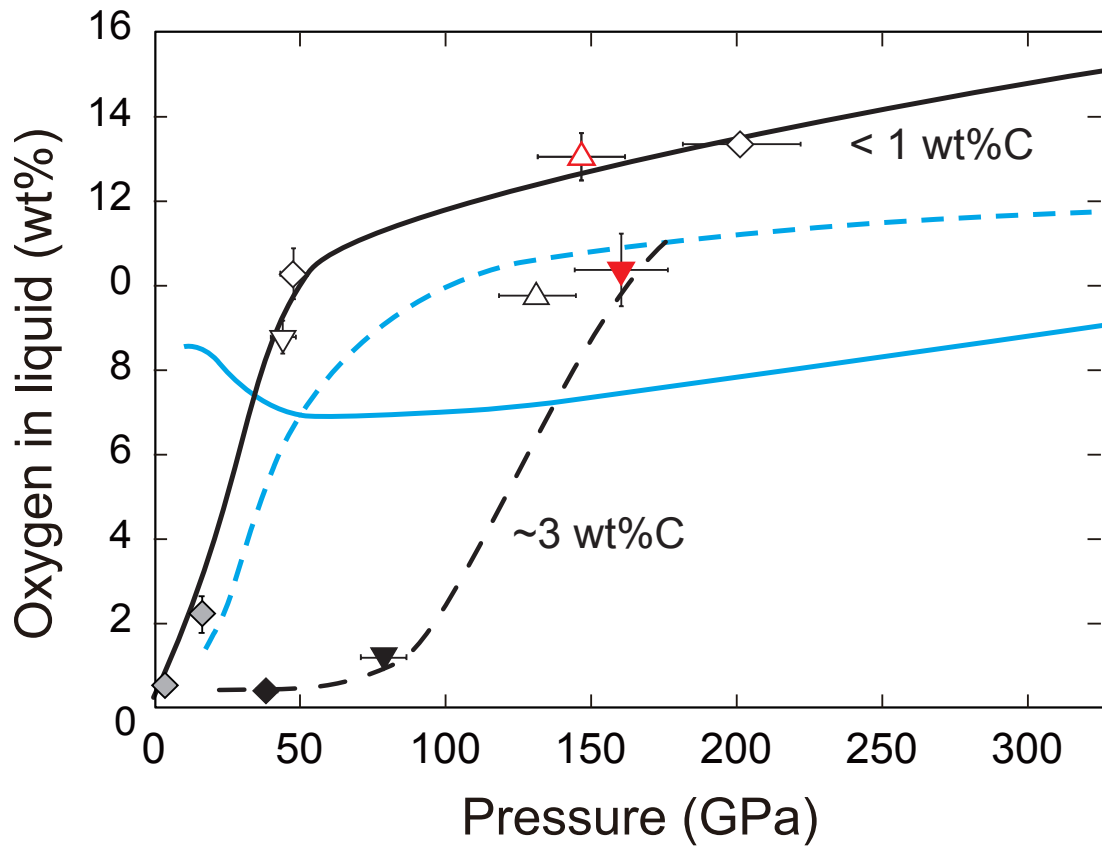


Figure S1. Liquid compositions obtained in melting experiments on the Fe-FeO \pm C system. Normal and reverse triangles, lower and upper bounds for O concentration in the Fe-FeO eutectic liquid, respectively; diamonds, the O contents in liquids coexisting both Fe and FeO (eutectic liquids). Red, this study (runs #A5 and #A6); black, Oka et al. (2019); gray, Ohtani et al. (1984) and Ringwood & Hibberson (1990). The black curves indicate changes in O concentration in liquids coexisting with Fe and FeO (solid line, with <1 wt% C in liquids; broken line, with ~3 wt% C in liquids). Blue dashed and solid curves represent thermodynamically-modelled eutectic liquid compositions in the Fe-FeO system assuming non-ideal and ideal solutions, respectively (Komabayashi, 2014).