

Adaptive monitoring of coral health at Scott Reef where data exhibit nonlinear and disturbed trends over time

Thilan AWLP^{1,2,3,9}, Fisher R^{4,5,6}, Thompson H^{1,2,3}, Menendez P^{7,8}, Gilmour J^{4,6}, and McGree JM^{1,2,3,*}

¹School of Mathematical Sciences, Faculty of Science, Queensland University of Technology (QUT), Australia

²Australian Research Council Centre of Excellence for Mathematical and Statistical Frontiers (ACEMS), Australia

³Centre for Data Science, QUT, Australia

⁴Australian Institute of Marine Science, Crawley, Australia

⁵Oceans Institute, University of Western Australia, Crawley, Australia

⁶Western Australian Marine Science Institution, Perth, Australia

⁷Department of Econometric and Business Statistics, Monash University, Australia

⁸Australian Institute of Marine Sciences, Townsville, Australia

⁹Department of Mathematics, University of Ruhuna, Sri Lanka

*Corresponding author:- Postal address: School of Mathematical Sciences, Faculty of Science, Queensland University of Technology, 2 George Street, Brisbane, QLD 4000; Tel: +61(0)410372540; Fax: +61 731382310; Email: james.mcgree@qut.edu.au

Abstract

1 Time series data are often observed in ecological monitoring. Frequently such
2 data exhibit nonlinear trends over time potentially due to complex relation-
3 ships between observed and auxiliary variables, and there may also be sudden
4 declines over time due to major disturbances. This poses substantial chal-
5 lenges for modelling such data and also for model-based adaptive monitoring.
6 We propose novel methods for finding adaptive designs for monitoring when
7 historical data show such nonlinear patterns and sudden declines over time.
8 This work is motivated by a coral reef monitoring program that has been
9 established at Scott Reef; a coral reef off the Western coast of Australia.

10 Data collected for monitoring the health of Scott Reef are considered,
11 and semiparametric and interrupted time series modelling approaches are
12 adopted to describe how these data vary over time. New methods are then
13 proposed that enable adaptive monitoring designs to be found based on such
14 modelling approaches. These methods are then applied to find future mon-
15 itoring designs at Scott Reef and form a set of recommendations for future
16 monitoring.

17 Through applying the proposed methods, it was found that future in-
18 formation gain is expected to be similar across a variety of different sites,
19 suggesting that no particular location needed to be prioritised at Scott Reef
20 for the next monitoring phase. In addition, it was found that omitting some
21 sampling sites/reef locations was possible without substantial loss in expected
22 information gain, depending upon the disturbances that were observed.

23 The resulting adaptive designs are used to provide recommendations for
24 future monitoring in this region, and for reefs where changes to the current
25 monitoring practices are being sought. Furthermore, as the methods used
26 and developed throughout this study are generic in nature, this research has
27 the potential to improve ecological monitoring more broadly where complex
28 data are being collected over time.

Keywords: Ecological monitoring, interrupted time series regression, mass
bleaching events, semiparametric regression, sudden declines in trends.

29 1. Introduction

30 Coral reefs are one of the most beautiful and biologically diverse ecosys-
31 tems globally. Unfortunately, environmental stressors such as severe cyclones
32 and bleaching exposures have had a negative impact on coral reefs (Gilmour
33 et al., 2019). As a result, the health of coral reefs are continually being mon-
34 itored to estimate the impact of such disturbances and to identify additional
35 vulnerabilities to decline.

36 In long-term coral reef monitoring, experimental design plays a vital role
37 in creating survey designs to collect data for assessing coral health, trends
38 over space and time, and to identify vulnerabilities of coral communities to
39 different disturbances (Campbell et al., 2001). Broadly, there are two types
40 of designs; static and adaptive. Static designs are those that do not change
41 over time (e.g. the same sites/reefs are visited each year), and have been
42 commonly used within monitoring programs. In contrast, adaptive designs
43 can vary over time based on, for example, information from new data, and
44 such methods have been proposed recently for determining when and where
45 to sample within a coral reef to learn about coral health (Kang et al., 2016).

46 In the context of adaptive design, the adaptation is primarily informed
47 by a statistical model. The purpose of this model is to extract informa-
48 tion contained within the historical data to quantify uncertainties about, for
49 example, the model itself, the model parameter values, and the response
50 variable of interest, and then utilise this information to guide future surveys.
51 For example, in Thilan et al. (2021), a spatial Beta regression model was

52 developed for coral cover, and used to find future adaptive designs. When
53 such designs were compared to those based on a linear model, the importance
54 of appropriately capturing trends and variability within historical data was
55 highlighted as this led to more informative and therefore efficient designs.

56 Ecosystems are subjected to a variety of observed and unobserved impacts
57 which may interact in a variety of different ways (Newbold et al., 2020). For
58 instance, coral reef ecosystems often exhibit nonlinear trends including sud-
59 den shifts due to mass coral bleaching, severe storms, and CoTS outbreaks
60 (Done, 1992, McCook, 1999). These nonlinear trends poses significant chal-
61 lenges in modelling ecological data (Oddi et al., 2019), and this challenge is
62 further exacerbated when there are sudden shifts in the overall trend due to
63 disturbances (Scheffer et al., 2001).

64 Generally, semiparametric regression modelling approaches provide more
65 flexibility than parametric models in describing a variety of relationships be-
66 tween (a function of) the mean response and given covariates (Crainiceanu
67 et al., 2005). Thus, the development and use of semiparametric regression
68 modelling approaches has received attention recently for modelling ecological
69 data (Vercelloni et al., 2014, 2017). However, currently no methods exist for
70 finding adaptive designs based on such models which limits how such infor-
71 mation can be used to guide future reef monitoring. In addition, to account
72 for sudden or sharp declines in the mean response due to disturbances such as
73 a mass bleaching event, approaches from time-series regression modelling can
74 be considered. Within a monitoring program, of further interest is then how

75 the coral reef should be sampled to estimate the impact of such a disturbance.

76 In this paper, we propose new methods to find adaptive designs when the
77 historical data exhibit nonlinear trends and sudden declines over time. The
78 motivation for this research is the improvement of the Scott Reef Research
79 Program (SRRP); a monitoring program of a coral reef system off the Western
80 coast of Australia. We leverage information from the historical data through
81 semiparametric and time series modelling approaches. Methods for finding
82 adaptive designs based on such a modelling approach are then proposed, and
83 designs are found under future monitoring scenarios at Scott Reef. These
84 designs are then evaluated and used to provide recommendations for future
85 surveys at Scott Reef and other reef monitoring programs where changes to
86 the sampling practices are being contemplated.

87 **2. Motivating example**

88 Scott Reef is located 270 kilometres off the current coast of North-Western
89 Australia (Gilmour and Smith, 2013) (Figure 1 (a)) and accordingly is iso-
90 lated from many human impacts. However, these reefs are frequently exposed
91 to cyclones and bleaching events. For example, due to elevated water temper-
92 atures over a few months in 1998, Scott Reef experienced a mass bleaching
93 event, resulting in a decline of coral up to 80% (Gilmour et al., 2019, Gilmour
94 and Smith, 2013) and thus, a complete change in coral cover trends was ob-
95 served over time (Figure A.1). Furthermore, such disturbance exposure does
96 not seem homogeneous across different survey locations. That is, there were

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97 survivors or relatively unharmed, moderately, and severely affected reef lo-
98 cations after this severe disturbance event (Figure A.2) (Gilmour and Smith,
99 2013). By adequately identifying the impacts of sudden disturbances, vari-
100 ations across the reef, and potential causes, it should be possible to develop
101 efficient and appropriate monitoring practices that can change/evolve over
102 time, and this is the aim of this paper.

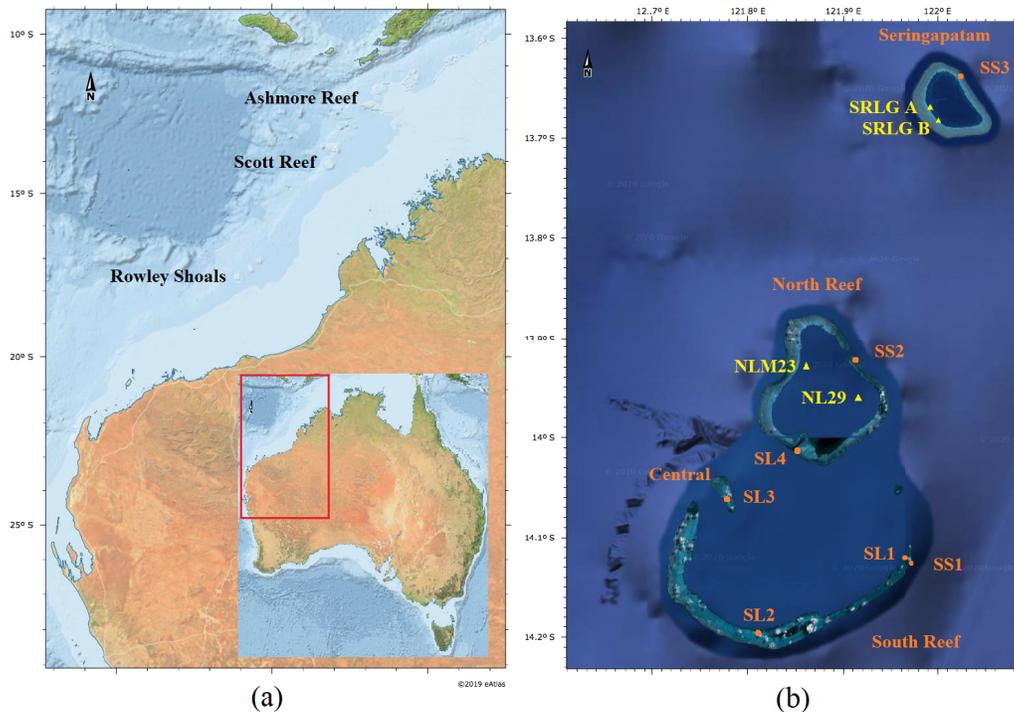


Figure 1: (a) The location of the system of Scott Reef and (b) the long-term monitoring sites located at South Reef, Central, North Reef, and Seringapatam (Google, n.d.). The orange points represent sites that have been surveyed since 1994 and the yellow triangles represent newly added sites after the 2016 bleaching event. “Bright Earth eAtlas basemap v1.0 (AIMS)”.

103 **3. Data**

104 The system of Scott Reef comprises of four separate structures, namely
105 North Reef, Central, South Reef, and Seringapatam (Figure 1 (b)). Under the
106 SRRP, data have been collected over six habitats called slope, upper slope,
107 crest, flat, lagoon, and outcrop from 1994.83 to 2017.92, where decimals
108 represent survey times within a given year, i.e. .83 denotes the 10th of 12
109 months. Three core sites have been sampled to collect data, which are nested
110 within each of seven reef locations (i.e. SL1, SL2, SL3, SL4, SS1, SS2, SS3)
111 (Figure 1 (b)). In this study, data collected between 1994.83 and 2016.08
112 were considered in accordance with future monitoring objectives at Scott
113 Reef (Section 4).

114 SRRP surveys are typically conducted in October but variations have
115 been observed from year to year (Table A.1). For instance, when there was
116 a severe disturbance, AIMS have collected data during, immediately after,
117 and then later in the year depending upon the nature of the disturbance.
118 In 1998, they conducted such pre- and post-bleaching surveys in January
119 and October, respectively, where there was interest in quantifying coral loss
120 during this time. When collecting disturbance data, AIMS has recorded
121 bleaching exposure (i.e. 0 = No coral bleaching, $1 \geq 1\%$ coral bleached) and
122 cyclone exposure in terms of the number of hours of reef system exposure to
123 damaging waves (Puotinen et al., 2016). Additionally, reef location-specific
124 cyclone and bleaching impacts have been documented.

125 4. Monitoring objectives

126 This study aims to develop recommendations for future monitoring at
127 Scott Reef and other reef monitoring programs where changes are being con-
128 sidered. We hope to achieve this goal through considering the following two
129 questions which form the basis for our two objectives:

- 130 (i) Are some reef locations (i.e. SL1, \dots , SS3) within Scott Reef more
131 important than others in providing information on coral health?
- 132 (ii) Which site at each reef location provides the most information about
133 coral health?

134 5. Design framework

135 5.1. Modelling historical data

136 *Capturing nonlinear trends*

137 Semiparametric regression approaches can be used to capture nonlinear
138 relationships within a regression model, and have been considered previ-
139 ously to describe data from coral communities on the Great Barrier Reef
140 (GBR) (Vercelloni et al., 2014). To outline our adopted modelling approach,
141 assume that $y_{srt} \sim \text{BIN}(n, p_{srt})$ where $n = 1250$ is the number of points
142 in a 250m combined length of transects, $p_{srt} = 1/(1 + \exp(-\mu_{srt}))$, and
143 $y_{srt} (s = 1, 2, 3; r = 1, \dots, 7; t = 1994.83, \dots, 2016.08)$ denotes the hard
144 coral cover at the s -th site, in the r -th reef location at t -th survey time.

145 Then, a semiparametric regression modelling approach can be used to model
146 the mean μ_{srt} as $\mu_{srt} = f(x_{srt})$, where x_{srt} are the survey times where data
147 have been collected from sites that are nested within reef locations, and f is
148 a smooth function.

149 There are different methods for modelling the smooth function, including
150 cubic splines, B-splines, truncated polynomials, radial splines etc (Crainiceanu
151 et al., 2005). We consider the low-rank thin-plate splines approach as it re-
152 quires fewer parameters to estimate, and also it is insensitive to the choice
153 of knots (Wood, 2003). Accordingly, the smooth function can be expressed
154 as follows:

$$f(x_{srt}, \boldsymbol{\theta}_0) = \beta_0 + \beta_1 x_{srt} + \sum_{k=1}^K \delta_k |x_{srt} - \eta_k|^3, \quad (1)$$

155 where $\boldsymbol{\theta}_0 = (\beta_0, \beta_1, \delta_1, \dots, \delta_K)^T$, β_0 is the intercept, β_1 is the regression
156 coefficient for time, $\boldsymbol{\delta} = (\delta_1, \dots, \delta_K)$ are random coefficients, η_k are knots,
157 and K is the total number of knots. The values of $|x_{srt} - \eta_k|$ are calculated
158 based on the sample quantile of x_{srt} 's (Crainiceanu et al., 2005).

159 Extensions to capture hierarchical structures within the data are straight-
160 forward via the inclusion of random effects, and such models can be defined
161 by considering random effects for sites nested within reef locations as follows:

$$\log(p_{srt}/(1 - p_{srt})) = \gamma_{sr} + \boldsymbol{\beta}_t \mathbf{z}_t + \boldsymbol{\beta}_d \mathbf{d}_r + f(x_{srt}, \boldsymbol{\theta}_0), \quad (2)$$

162 where γ_{sr} represents the corresponding nested random effect that follow a
163 distribution $p(\gamma_{sr}|\lambda_r, \log \sigma_s)$ where $\lambda_r \sim p(\lambda_r|\log \sigma_r)$, where $\log \sigma_s$ and $\log \sigma_r$
164 are the corresponding site and reef random effects standard deviations in log
165 scale, respectively. Wood (2003) describes the extension of such a model to
166 accommodate the other potential covariates, and we follow this approach to
167 incorporate bleaching exposure and cyclone hours. These covariates vary over
168 time for the whole reef system, and thus are hereafter referred to as time-
169 varying covariates. In Equation (2), \mathbf{z}_t represents time-varying covariates
170 and $\boldsymbol{\beta}_t$ is the corresponding vector of regression coefficients. Additionally, we
171 incorporated three dummy variables to account for cyclone, severe cyclone,
172 and bleaching exposures at different reef locations. The corresponding data
173 matrix and the vector of regression coefficients are denoted as \mathbf{d}_r and $\boldsymbol{\beta}_d$,
174 respectively.

175 *Accounting sudden declines in trends*

176 Coral cover is often impacted by disturbances such as cyclones and bleach-
177 ing events, and some major events will result in sudden declines in coral cover
178 trends (De'ath et al., 2012, Osborne et al., 2011). We propose that estimat-
179 ing the impact of such major events can be achieved using an interrupted
180 time series (ITS) regression approach (Bernal et al., 2017, Linden, 2015). In

181 general, an ITS approach can account for sudden changes in the trend due
 182 to some intervention introduced or disturbance that has occurred (McDowall
 183 et al., 2019). When applying ITS, the type of impact due to the distur-
 184 bance should be hypothesised. This may include a gradual change in slope
 185 or in both the intercept and slope within the model for the mean response
 186 (Bernal et al., 2017). In addition, some disturbances may cause an immedi-
 187 ate change in the trend, but others may have a lag period before any effect
 188 appears. The reader is referred to Bernal et al. (2017) for more details about
 189 modelling different types of sudden changes in time-series data.

190 Based on coral cover trends over time (Figure A.1), we hypothesised that
 191 the 1998 mass bleaching event resulted in both changes to the intercept and
 192 slope when modelling coral cover trajectories. Furthermore, it was proposed
 193 that the impact existed for years as mortality does not happen completely
 194 during or a few months after bleaching (Gilmour and Smith, 2013, Baird and
 195 Marshall, 2002). The model defined previously using Equation (2) can now
 196 be extended to accommodate such an impact as follows:

$$\begin{aligned} \log(p_{srt}/(1-p_{srt})) = & \gamma_{sr} + \beta_t \mathbf{z}_t + \beta_d \mathbf{d}_r + f(x_{srt}, \boldsymbol{\theta}_0) + \beta_l \text{BLE98}_{srt} \\ & + \beta_s \text{Time98}_{srt}, \end{aligned} \quad (3)$$

197 where BLE98_{srt} represents the bleaching impact, i.e. $\text{BLE98}_{srt} = 0$ before the
 198 bleaching event happened and otherwise it is equal to 1, β_l is the level change
 199 due to the bleaching impact. Here, Time98_{srt} represents the time before and

200 after the bleaching event, i.e. $\text{Time98}_{srt} = 0$ before the bleaching event
201 occurred, and after that, time increases with survey time, and β_s represents
202 the corresponding slope change.

203 In the model, cyclone hours data were count values that varied over a
204 large range; thus, the square-root transformation (Weber, 1990) was applied
205 before including this covariate into the model. This transformation was also
206 applied to ensure a linear relationship was appropriate between cyclone hours
207 and $\log(p_{srt}/(1 - p_{srt}))$ (O’Hara and Kotze, 2010). Previous studies have
208 considered centring covariates to avoid numerical issues when fitting a given
209 model, and we follow this approach for the time-varying covariates (Selig
210 et al., 2012, Vercelloni et al., 2014). Furthermore, we calculated $|x_{srt} - \eta_k|$
211 by considering the centered time (Crainiceanu et al., 2005).

212 *Approximating the posterior distribution*

213 Within a Bayesian framework, we are interested in estimating the joint
214 posterior distribution $p(\boldsymbol{\theta}, \boldsymbol{\xi} \mid \mathbf{y}_p, \mathbf{z}_p, \mathbf{v}_p, \mathbf{d}_p)$ of model parameters and random
215 effects, where $\boldsymbol{\theta} = (\beta_0, \beta_1, \boldsymbol{\beta}_t, \boldsymbol{\beta}_d, \beta_l, \beta_s, \boldsymbol{\delta}, \log \sigma_\delta, \log \sigma_r, \log \sigma_s)$ denotes all
216 parameters in the model (Equation (3)), $\boldsymbol{\xi}$ is a matrix representation for the
217 nested random effects, \mathbf{d}_p denotes previously used static survey designs at
218 Scott Reef, \mathbf{v}_p represents data matrices related to $|x_{srt} - \eta_k|$ and the inter-
219 rupted component (i.e. BLE98_{srt} and Time98_{srt}), \mathbf{y}_p denotes the collected
220 coral cover data, and \mathbf{z}_p is the collected time-varying covariates, where we
221 have shifted notation such that all previously collected data will be indexed

222 by p . This will be convenient when considering future monitoring scenarios,
223 see later. To estimate the posterior distribution (see Appendix A.3 for more
224 details), Markov Chain Monte Carlo (MCMC) methods can be used. For
225 this purpose, WinBUGS was used (Lunn et al., 2000).

226 *Model selection*

227 To find the most appropriate model to describe the previously collected
228 data at Scott Reef, we considered the \mathcal{M} -closed perspective of Bernardo
229 and Smith (2009). Accordingly, the most appropriate model for the data
230 is assumed to be contained within a finite set of L candidate models $\{m \in$
231 $1, 2, \dots, L\}$. We defined the class of models by considering the following com-
232 ponents: the nested random effects for sites within reef locations (NRE); a
233 smooth component (SC); all the available covariates (ALL COV), i.e. Time,
234 Bleaching, Cyclone hours, Interrupted 98 (i.e. BLE98_{srt} and Time98_{srt}),
235 location-specific covariates impacts, i.e. Cyclone Loc2 (i.e. Cyclone Loc and
236 Severe cyclone Loc) and Bleaching Loc, and the interaction between Bleach-
237 ing and Cyclone. The most appropriate model within this class was then
238 determined via the deviance information criterion (DIC) with a preference
239 for the model with the smallest of these values (Spiegelhalter et al., 2014).
240 Prior information was specified to be vague on likely range of values of each
241 parameter (Table A.2). In addition, to appropriately capture the nonlinear
242 features of the data, a specific number of knots needs to be determined. For
243 this, we followed the approach of Ruppert (2002) where the number of knots

244 was increased until there was little to no improvement in model fit. This
245 resulted in the use of three knots.

246 *5.2. Adaptive design*

247 We consider a Bayesian inference framework for undertaking adaptive de-
248 sign as it supports the incorporation of knowledge gained through previously
249 collected data to guide future sampling via a prior distribution. The prior
250 that was used for this study was the posterior distribution for the model
251 that was found to be most appropriate for the collected data. Based on this
252 prior information, the value of a design with respect to a given monitoring
253 objective can be evaluated as described below.

254 *Quantifying designs*

255 Define a design as $\mathbf{d} = (\mathbf{d}_1, \mathbf{d}_2, \dots, \mathbf{d}_{n_s})$, where n_s is the number of sites
256 appearing in a new design out of all sites (i.e. 7 reef locations \times 3 sites = 21
257 sites). The usefulness of such a design \mathbf{d} can be quantified via what is called
258 a utility function which evaluates how much information will be provided
259 from data \mathbf{y} to address a specific monitoring objective. As it is unknown
260 what data will be observed, the expectation of the utility function is taken
261 with respect to this and other unknowns as follows:

$$E[u(\mathbf{d}, \mathbf{z}, \mathbf{y}|\mathbf{y}_p, \mathbf{z}_p, \mathbf{v}_p, \mathbf{d}_p)] = \int_{\mathbf{y}} u(\mathbf{d}, \mathbf{z}, \mathbf{y}|\mathbf{y}_p, \mathbf{z}_p, \mathbf{v}_p, \mathbf{d}_p) p(\mathbf{y}|\mathbf{z}, \mathbf{d}, \mathbf{y}_p, \mathbf{z}_p, \mathbf{v}_p, \mathbf{d}_p) d\mathbf{y}, \quad (4)$$

262 where \mathbf{z} represents specific values of the time-varying covariates which define
263 particular future monitoring scenarios. Further details about these scenarios
264 will be provided later in this section.

265 The choice of a utility function depends on the monitoring objective.
266 Here, our goal is to determine the relative importance of survey locations
267 for providing information about coral health based on a statistical model.
268 This suggests we are interested in the precise estimation of parameters in the
269 adopted model so that, for example, we can precisely quantify the impact
270 of each disturbance. Thus, we chose the Kullback-Leibler divergence (KLD)
271 (Kullback and Leibler, 1951), which is a specific utility for the parameter
272 estimation. The KLD utility function can be expressed as follows (Friel and
273 Pettitt, 2008):

$$\begin{aligned} u(\mathbf{d}, \mathbf{y}, \mathbf{z} | \mathbf{y}_p, \mathbf{z}_p, \mathbf{v}_p, \mathbf{d}_p) &= \int_{\boldsymbol{\theta}} \int_{\boldsymbol{\xi}} p(\boldsymbol{\theta}, \boldsymbol{\xi} | \mathbf{y}, \mathbf{z}, \mathbf{y}_p, \mathbf{z}_p, \mathbf{v}_p, \mathbf{d}, \mathbf{d}_p) \\ &\quad \times \log p(\mathbf{y} | \boldsymbol{\theta}, \boldsymbol{\xi}, \mathbf{z}, \mathbf{y}_p, \mathbf{z}_p, \mathbf{v}_p, \mathbf{d}, \mathbf{d}_p) d\boldsymbol{\xi} d\boldsymbol{\theta} \\ &\quad - \log p(\mathbf{y} | \mathbf{z}, \mathbf{z}_p, \mathbf{y}_p, \mathbf{v}_p, \mathbf{d}, \mathbf{d}_p). \end{aligned} \quad (5)$$

274 Evaluating this utility thus measures how much the posterior distribution
275 diverges from the prior. In terms of designs, a larger deviation for a given
276 design \mathbf{d} indicates more has been learned from data collected according to
277 that design. Thus, we seek a design \mathbf{d} that maximises the expectation given
278 in Equation (4) where the utility is defined in Equation (5).

279 To find an optimal design, we need to evaluate the expected utility. How-
 280 ever, typically this expression does not have a closed-form solution. Thus, a
 281 numerical approximation is required. One can use the Monte Carlo integra-
 282 tion (Ryan, 2003) for this purpose which can be defined as follows:

$$E[u(\mathbf{d}, \mathbf{y}, \mathbf{z} | \mathbf{z}_p, \mathbf{y}_p, \mathbf{v}_p, \mathbf{d}_p)] \approx \frac{1}{J} \sum_{j=1}^J u(\mathbf{d}, \mathbf{y}^{(j)}, \mathbf{z} | \mathbf{z}_p, \mathbf{y}_p, \mathbf{v}_p, \mathbf{d}_p), \quad (6)$$

283 where $J (\geq 100)$ is the controlling parameter for Monte Carlo integration.

Algorithm 1: Approximate the expected utility

1. Initialise $\mathbf{d}, \mathbf{y}_p, \mathbf{z}_p, \mathbf{v}_p, \mathbf{d}_p, \mathbf{z}, t, J$
 2. For $j = 1$ to J do
 3. Simulate $\boldsymbol{\theta}^{(j)}, \boldsymbol{\xi}^{(j)} \sim p(\boldsymbol{\theta}, \boldsymbol{\xi} | \mathbf{y}_p, \mathbf{z}_p, \mathbf{v}_p, \mathbf{d}_p)$
 4. Simulate $\mathbf{y}^{(j)} \sim p(\mathbf{y} | \boldsymbol{\theta}^{(j)}, \boldsymbol{\xi}^{(j)}, \mathbf{z}, \mathbf{y}_p, \mathbf{z}_p, \mathbf{v}_p, \mathbf{d}_p)$ at the next survey time t
 based on \mathbf{d} via a Taylor series approximation to the mean response
 5. Estimate $p(\boldsymbol{\theta}, \boldsymbol{\xi} | \mathbf{y}, \mathbf{z}, \mathbf{y}_p, \mathbf{z}_p, \mathbf{v}_p, \mathbf{d}, \mathbf{d}_p)$ via Laplace approximation
 6. Evaluate KLD utility $u(\mathbf{d}, \mathbf{z}, \mathbf{y}^{(j)} | \mathbf{z}_p, \mathbf{y}_p, \mathbf{v}_p, \mathbf{d}_p)$
 7. Store $u(\mathbf{d}, \mathbf{z}, \mathbf{y}^{(j)} | \mathbf{z}_p, \mathbf{y}_p, \mathbf{v}_p, \mathbf{d}_p)$
 8. End for
 9. Output $E[u(\mathbf{d}, \mathbf{z}, \mathbf{y} | \mathbf{z}_p, \mathbf{y}_p, \mathbf{v}_p, \mathbf{d}_p)] \approx \frac{1}{J} \sum_{j=1}^J u(\mathbf{d}, \mathbf{z}, \mathbf{y}^{(j)} | \mathbf{z}_p, \mathbf{y}_p, \mathbf{v}_p, \mathbf{d}_p)$
-

284 *Approximating the expected utility*

285 The approach to approximate the expected utility is outlined in Algorithm
286 1, which begins by initialising some parameters (line 1). To approximate the
287 expected utility for a given design \mathbf{d} , many data sets need to be simulated
288 based on the given design (line 2). For this purpose, we simulate parameter
289 and random effect values from the prior distribution (line 3). To simulate
290 coral cover for the next survey time point t (line 4), we propose the Taylor
291 series expansion around the mean at the last survey point, i.e. 2016.08 (Table
292 A.6). In such a case, a bivariate Taylor series expansion needs to be applied as
293 the regression model includes two time variables following the incorporation
294 of the interrupted regression component. For the given model, the Taylor se-
295 ries approximation can be described as follows: $f(x_{srt}, \text{Time98}_{srt}) \approx f(a, b) +$
296 $f_{x_{srt}}(a, b)(x_{srt} - a) + f_{\text{Time98}_{srt}}(a, b)(\text{Time98}_{srt} - b)$, where $f(x_{srt}, \text{Time98}_{srt})$
297 is the value of the function at the next survey point (i.e. $t = 2016.33$) and
298 (a, b) are values which with the Taylor series is centered (see Appendix A.7
299 for extrapolation results). The posterior distribution needs to be approxi-
300 mated for each simulated data set (line 5). Given this needs to be performed
301 a large number of times, this is a computationally demanding step in the
302 algorithm. To address this, a Laplace approximation (Overstall et al., 2018)
303 was adopted. Given this approximation to the posterior distribution, the
304 KLD utility can be evaluated (see Appendix A.9 for more details) (lines 6-
305 7). Finally, an average of KLD utility values is used to approximate the
306 expected utility value (line 9).

307 *Finding optimal designs*

308 We are now able to approximate the expected utility of a given design \mathbf{d} .
309 The next step is to find the optimal design \mathbf{d}^* out of the set of candidate de-
310 signs which maximises the expected utility, i.e. $\mathbf{d}^* = \arg \max_{\mathbf{d}} E[u(\mathbf{d}, \mathbf{z}, \mathbf{y} | \mathbf{z}_p,$
311 $\mathbf{y}_p, \mathbf{v}_p, \mathbf{d}_p)]$. Here, candidate designs need to be formulated in accordance
312 with monitoring objectives. As far as Objective (i) is concerned, we will in-
313 vestigate whether some reef locations within Scott Reef have greater utility
314 than others. Accordingly, seven candidate designs were formulated consid-
315 ering all possible combinations where six out of seven reef locations will be
316 sampled. The corresponding designs were labelled as SL1, \dots , SS3 where
317 for example, design SL1 denotes that no data will be collected from the reef
318 location SL1 for the next survey time. As there will be a fixed number of
319 potential candidate designs (i.e. seven) under this objective, we will enu-
320 merate all possible designs to determine the optimal. Next, under Objective
321 (ii), we determine the optimal design consisting of the most informative site
322 (out of the three) at each reef location. To locate these optimal designs,
323 the coordinate-exchange algorithm was used based on five randomly selected
324 initial designs (Meyer and Nachtsheim, 1995).

325 To evaluate our adaptive designs, two disturbance scenarios (i.e. two
326 different values for \mathbf{z}) were considered. These were: (a) actual covariate
327 data collected at the next survey time (i.e. 2016.33) and (b) bleaching and
328 cyclone impacts including an interaction between them at each reef location
329 (see Appendix A.8 for more details). This means that Scenario (a) withdraws

330 the prevailing cyclone exposure while Scenario (b) includes cyclone location
 331 disturbances and cyclone-bleaching interactions for each reef location. Each
 332 objective defined previously will be assessed under these two disturbance
 333 scenarios.

334 6. Results

335 6.1. Modelling historical data from Scott Reef

336 *Model selection*

337 To select the most appropriate model for Scott Reef hard coral cover
 338 data, we defined the class of models by considering all components described
 339 in Section 5.1. The corresponding model comparison results based on DIC
 340 are provided in Table A.3. As the model with a smaller value of DIC is
 341 preferred, the most appropriate model found for coral cover can be described
 342 as follows:

$$\begin{aligned}
 \log(p_{srt}/(1 - p_{srt})) = & \beta_0 + \beta_1 \text{Time} + \beta_2 \text{Bleaching}_t + \beta_3 \text{Cyclone hours}_t \\
 & + \beta_4 \text{Bleaching} \times \text{Cyclone}_{rt} + \beta_5 \text{BLE98}_t + \beta_6 \text{Time98}_t \\
 & + \beta_7 \text{Cyclone Loc}_{rt} + \beta_8 \text{Severe cyclone Loc}_{rt} \quad (7) \\
 & + \beta_9 \text{Bleaching Loc}_{rt} + \delta_1 v_{1,rst} + \delta_2 v_{2,rst} + \delta_3 v_{3,rst} + \gamma_{sr},
 \end{aligned}$$

343 where $\beta_i, i = 1, \dots, 9$ are the regression coefficients and δ_1, δ_2 , and δ_3 are
 344 random coefficients. The goodness-of-fit of this model was assessed and found

345 to be appropriate, see Appendix A.6 for further details.

346 *6.2. Adaptive design*

347 *Importance of reef locations*

348 Under Objective (i), we aim to determine the relative importance of seven
349 reef locations at Scott Reef. Firstly, the disturbance Scenario (a) is consid-
350 ered. For this evaluation, we formulated seven designs (i.e. SL1, \dots , SS3),
351 as described in Section 5.2. To evaluate these designs, the KLD mean ex-
352 pected utility values were evaluated. These results are shown in Figure 2 (a),
353 where the y-axis represents the efficiency of each design with respect to the
354 design where all reef locations were included for survey at the next survey
355 time point. These design efficiencies were found with respect to sampling all
356 seven reef locations by evaluating the expected utility of each design 20 times,
357 and taking the average (see Appendix A.10 for more details). A summary of
358 utility evaluations is given in Table 1 to aid in interpretation.

359 According to Table 1, SL3 is the optimal design as it has the highest
360 mean efficiency. As the missing reef location within this design is SL3, this
361 reef location can be considered as the least informative reef location under
362 Scenario (a). This suggests that less information is expected to be lost by
363 omitting reef location SL3 compared to omitting any other reef locations.
364 Similarly, the reef location SL2 can be reported as the most informative reef
365 location as omitting this reef location resulted in the largest efficiency reduc-
366 tion (Table 1). However, it should be noted that there is very little difference

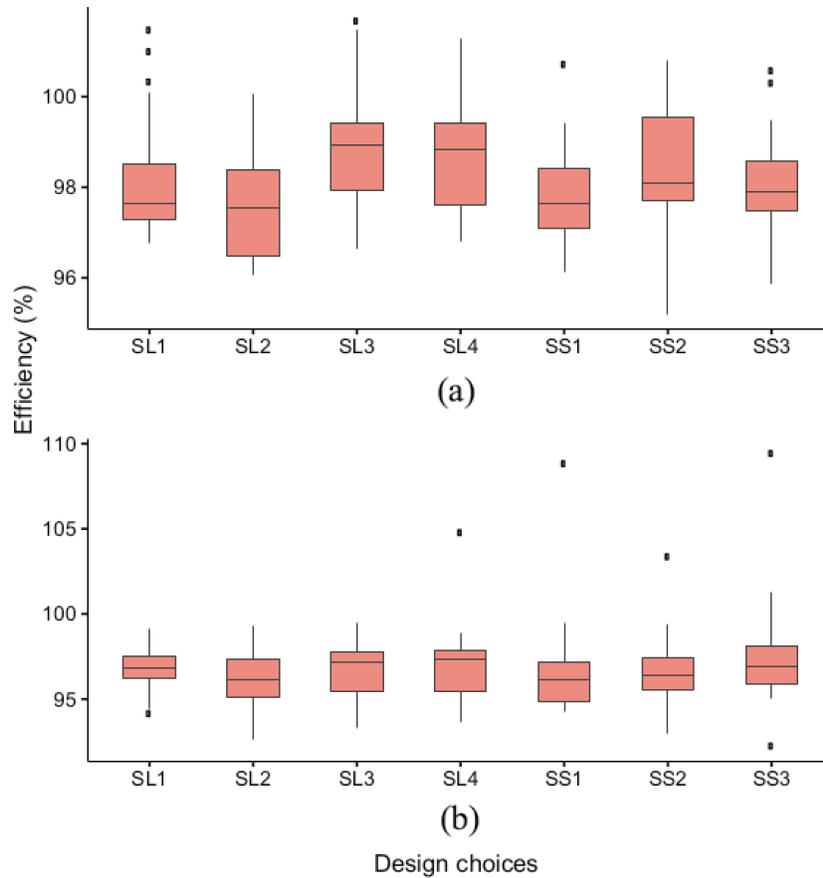


Figure 2: Utility evaluations results under disturbance Scenario (a) and (b) for seven designs (x-axis). y-axis represents efficiency calculated against the design that included all seven reef locations.

367 in the efficiency values between reef locations (Figure 2 (a)). Indeed, some
 368 of the differences observed could potentially be due to Monte Carlo error.

369 Secondly, we evaluate Objective (i) under the disturbance Scenario (b).
 370 The corresponding utility evaluation results and summary are provided in
 371 Figure 2 (b) and Table 2, respectively. It is evident from Figure 2 (b) that
 372 all the reef locations have similar median efficiency values under Scenario

Table 1: Summary of utility evaluations for seven designs under Scenario (a) in Objective (i).

Design	Mean efficiency (%)	Standard deviation
SL1	98.213	1.399
SL2	97.579	1.195
SL3	98.876	1.395
SL4	98.774	1.290
SS1	97.818	1.082
SS2	98.420	1.354
SS3	98.054	1.176

373 (b). The design SS3 has the highest efficiency; thus, the reef location SS3
374 can be reported as the least informative reef location under Scenario (b).
375 Furthermore, comparing Figure 2 (a) and (b) shows that there are similar
376 efficiency for designs under the two disturbance scenarios considered. This
377 suggests that the optimal design is robust to the two scenarios considered
378 under Objective (i).

379 To explore these design selections, consider that the posterior means $\theta_{m_1}^*$
380 will be similar to the prior means $\theta_{m_0}^*$, so this should not particularly con-
381 tribute to the optimal design selection under KLD utility function, see Equa-
382 tion (A.1). Accordingly, these design selections could be driven by the pos-
383 terior variance-covariance of the parameters. Upon investigating this, the
384 larger utility values appeared to be related to the estimation of the reef ran-
385 dom effect standard deviation parameter (i.e. $\log \sigma_r$). This is typically where

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Table 2: Summary of utility evaluations for seven designs under Scenario (b) in Objective (i).

Design	Mean efficiency (%)	Standard deviation
SL1	96.708	1.302
SL2	96.205	1.682
SL3	96.775	1.612
SL4	97.064	2.360
SS1	96.699	3.145
SS2	96.663	2.108
SS3	97.474	3.369

386 the largest change from the prior was observed, and thus could potentially
 387 be driving the design selection i.e. designs that provide more information on
 388 the variability of reef locations are being preferred.

Table 3: Summary of utility evaluations under each disturbance scenario in Objective (ii).

Design	Mean efficiency (%)	Standard Deviation
Scenario (a)	86.285	5.492
Scenario (b)	71.184	2.616

389 *Informative sites at each reef location*

390 Under Objective (ii), we determine the optimal design that consists of
 391 the most informative site at each reef location subject to two disturbance

392 scenarios. The mean efficiency values of each optimal design are provided
393 in Table 3. The selected sites from each reef location into the optimal de-
394 signs under the two scenarios are reported in Table A.7. It can be seen
395 from the table that the optimal designs contain different site combinations
396 under the two scenarios. It was found through investigating these optimal
397 designs that the estimation of $\log \sigma_r$ was a main contributor to these optimal
398 design selections. This indicates that the optimal site combination under a
399 given disturbance scenario provides more information about the between reef
400 variability.

401 The optimal designs under the two scenarios have the mean efficiency
402 values of 86.285% and 71.184% respectively (Table 3). It is evident from
403 these a considerable reduction in mean efficiency under Scenario (b). This
404 indicates that if disturbances are similar to previous years, then minimal
405 sampling (i.e. one site per reef location) will capture a substantial proportion
406 of information. However, when a variety of disturbance combinations are
407 observed, then there appears to be more information lost, so there might be
408 value to undertaking additional sampling in such cases.

409 **7. Discussion**

410 The present study was designed to develop adaptive design methods us-
411 ing semiparametric and ITS models and utilised prior knowledge captured
412 through such methods to guide future surveys at Scott Reef. We demon-
413 strated the use of such a modelling approach in finding adaptive design when

414 data show nonlinear trends with some sudden shifts over time. For this pur-
415 pose, it was shown that changes around major environmental disturbances
416 in ecological monitoring could be accounted for using an ITS regression mod-
417 elling approach. This enabled prior information from historical data to be
418 appropriately formed when such data potentially exhibit complex ecological
419 relationships.

420 We assessed the importance of reef locations under Objective (i) subject
421 to two disturbance scenarios. The results showed that there was very little
422 difference between the selection of which reef location to omit under any of
423 the scenarios. This indicates that the design choice is relatively inconsequen-
424 tial. Also, dropping one reef location resulted in very little information loss,
425 allowing the survey effort to be reduced without losing a substantial amount
426 of information about the parameters in the developed model.

427 Under Objective (ii), we found the optimal designs consisting of one site
428 at a given reef location based on two disturbance scenarios. This provides
429 insight into the most appropriate site to sample from a given reef location
430 depending on prevailing disturbance conditions. The differences between the
431 optimal designs between these two scenarios suggests that site selection de-
432 pends on the disturbances that have been observed, and our methods provide
433 a framework with which to make this decision.

434 In terms of modelling monitoring data, the Gompertz model has been
435 considered recently (MacNeil et al., 2019) for capturing nonlinear relation-
436 ships in population growth. However, such a model proved to not be flexible

437 enough to capture nonlinear trends where observations have been collected
438 with unequal time gaps. In such circumstances, semiparametric modelling
439 approaches can be utilized to capture nonlinear trends, as demonstrated in
440 this study. The consideration of such a modelling approach meant that new
441 design methods needed to be proposed such that adaptive designs could be
442 found in this context. This was demonstrated by considering two future dis-
443 turbance scenarios, and assessing the performance of these designs against
444 more resource intensive sampling.

445 In terms of future research directions, we did not consider uncertainty
446 about future disturbances but instead considered how the optimal design
447 choice changed depending on the given disturbance conditions. If one were
448 to do so, it might yield robust designs over various disturbance patterns. The
449 use of this will most likely be dependent on a given year. Indeed, it is likely
450 that it will be known if a severe cyclone and mass bleaching has occurred
451 at Scott Reef, but data on the occurrence of other disturbances may not be
452 readily available.

453 **Recommendations for future reef monitoring based on findings** 454 **from Scott Reef**

455 (i) Pre-assessment of the expected information gain by location (e.g. site
456 or reef location) can be used to determine if any locations can be pri-
457 oritised for data collection. Here, it was found that information gain
458 from sites was similar, so no particular location needed to be prioritised
459 over another.

- 460 (ii) After an extensive monitoring period, explore reduced sampling prac-
461 tices as there is potential to reduce sampling effort (e.g. drop site or
462 reef location) without experiencing significant information loss about
463 coral health.
- 464 (iii) Evaluate disturbance patterns at monitoring locations as these can in-
465 fluence information gain e.g. here it was shown that more information
466 about coral health was obtained when new disturbance patterns were
467 experienced when compared to historical disturbance patterns.
- 468 (iv) On-going review of monitoring practices is recommended to assess ef-
469 fectiveness of adaptive designs

470 **8. Acknowledgements**

471 Thilan AWLP was supported by the Australian Technology Network of
472 Universities Industry Doctoral Training Centre (ATN IDTC) Scholarship.
473 McGree JM was supported by an Australian Research Council Discovery
474 Project (DP200101263). We would like to thank the ACEMS, the AIMS
475 and QUT Centre for Data Science. Historical data was collected by AIMS
476 with funding from Woodside as operator for and on behalf of the Browse
477 Joint Venture. Also, we would like to acknowledge computer resources and
478 services such as HPC provided by QUT. And finally, thanks to Nicole Ryan

479 for her help regarding Scott Reef data. Author contributions: Thilan AWLP,
480 McGree JM, and Fisher R designed the research; Thilan AWLP performed
481 the research and wrote the paper; Fisher R, Thompson H, Menendez P, and
482 McGree JM provided research conception and critical review of manuscript
483 drafts. Gilmour J contributed through conceptualisation and the acquisition
484 of the SRRP data. Further, we have no conflicts of interest to disclose.

485 **9. Additional information**

486 *9.1. Data availability*

487 The access to data that support the findings of this study are available
488 through the below link from the corresponding author, Thilan AWLP, upon
489 reasonable request. Giving such access requires prior approval from the Aus-
490 tralian Institute of Marine Science who owns these data:

491 <https://doi.org/10.5281/zenodo.4574062>

492 *9.2. Computer code*

493 All code to reproduce the analysis can be found through the following
494 DOI:

495 <https://doi.org/10.5281/zenodo.4586187>

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