

Rubber Fibre Composite Modelling and its Influence on Fatigue Damage Assessment

Simon Oman¹, Marko Nagode², and Jernej Klemenc²

¹University of Ljubljana, Faculty of Mechanical Engineering

²University of Ljubljana

August 11, 2020

Abstract

A novel multi-axial energy-based approach is presented and used to demonstrate the influence of different finite element (FE) modelling techniques on the prediction of the fatigue life of a rubber composite with long oriented fibres. It is shown that the simplest modelling methods using 2D elements with rebar layers, layered 2D elements or layered 3D elements do not allow for a precise determination of the critical location and damage value. In contrast, modelling methods with 3D matrix and discrete reinforcement provide much better results. The predicted critical location corresponds to the measured one, although the predicted fatigue life still differs from the measured results. The most complex microscopic modelling method shows the best agreement between the predicted and measured fatigue life. Since microscopic modelling is not suitable for modelling larger products made of rubber fibre composite, it is also noted that modelling techniques with 3D matrix and discrete reinforcing elements can be used with the same accuracy if the fatigue life curve is obtained from measurements on the specimens made of composite material rather than the specimens made of the critical base material (rubber).

Hosted file

Manuscript.docx available at <https://authorea.com/users/349921/articles/475134-rubber-fibre-composite-modelling-and-its-influence-on-fatigue-damage-assessment>

Material Model	Hyperelastic Marlow (defined by uniaxial test)		Elastic	Transversely isotropic elastic	Orthotropic elastic
Section	Rubber matrix		Rebar layers + truss elements	Sections of reinforced material - micro model	Reinforcement plies - mixed modelling
Parameters	Nom. Stress [MPa]	Strain [1]	$E=2300\text{MPa}$ $\nu=0.45$	$E_1=20\text{MPa}$ $E_2=20\text{MPa}$ $E_3=2300\text{MPa}$ $\nu_{12}=0.45$ $\nu_{13}=0.004$ $\nu_{23}=0.004$ $G_{12}=6.896\text{MPa}$ $G_{13}=50\text{MPa}$ $G_{23}=50\text{MPa}$	$E_1=1800\text{MPa}$ $E_2=1\text{MPa}$ $E_3=1\text{MPa}$ $\nu_{12}=0.002$ $\nu_{13}=0.002$ $\nu_{23}=0.45$ $G_{12}=0.33\text{MPa}$ $G_{13}=0.33\text{MPa}$ $G_{23}=0.345\text{MPa}$
	0	0			
	0.2738	0.1346			
	0.4467	0.2607			
	0.5717	0.4004			
	0.6721	0.5365			
	0.7427	0.6699			
	0.8150	0.8017			
	0.9336	0.9288			
	1.0867	1.0696			

Modelling technique	U_{ae}^{cycle} [J/mm ³]	Fatigue life N [cycles]
2D structural matrix with rebar layers	0.224	2.5×10^8
3D matrix + embedded 2D surface elements with rebar layer	0.294	5.4×10^7
3D matrix + 2D surface elements with rebar layer	0.334	2.63×10^7
3D matrix + embedded 1D truss elements	0.250	1.35×10^8
2D mixed modelling	0.058	5.11×10^{11}
3D mixed modelling	0.054	7.64×10^{11}
Complete 3D micro modelling	0.540	1.75×10^6
Measured results (average)	/	1.92×10^6

ENERGY BASED FATIGUE DAMAGE CALCULATION (POSTPROC)

FINITE ELEMENT ANALYSIS













